


DYNASTEE


DYNamic Analysis, Simulation and Testing
applied to the **E**nergy and **E**nvironmental
performance of buildings

Free On-Line Training Webinars; 22 and 29 September, 6 and 13 October 2021


Dynamic Calculation Methods for Building Energy Performance Assessment

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Denmark







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1



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2



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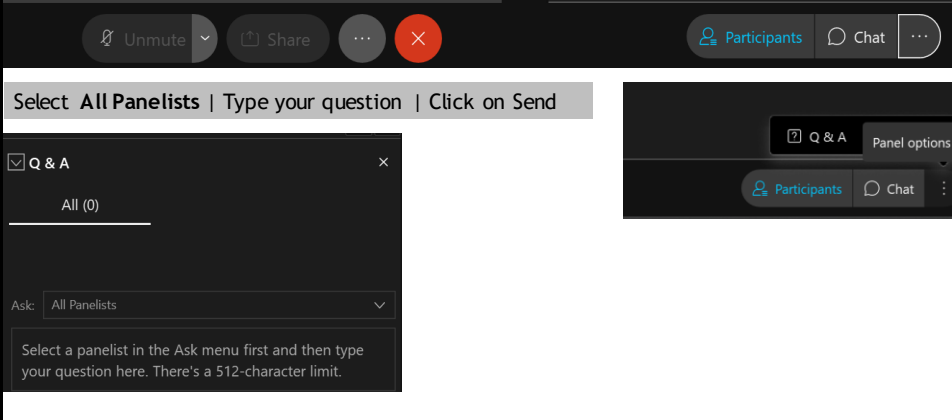
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3



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NOTES:

1. The questions addressed to the speakers during this webinar- via the Q&A box- will be gathered and answered **during the last webinar of the series on October 13th**
2. After the end of the webinar you can also send further questions you might have, via email to Hans Bloem at: hans.bloem@inive.org
3. The webinar will be recorded and published at <https://dynastee.info/> within a couple of weeks, along with the presentation slides.

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4



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2nd Webinar 29th September 2021

María José Jiménez



Paul Baker



University for the Common Good

Webinar management



Maria Kapsalaki
(INIVE, BE)

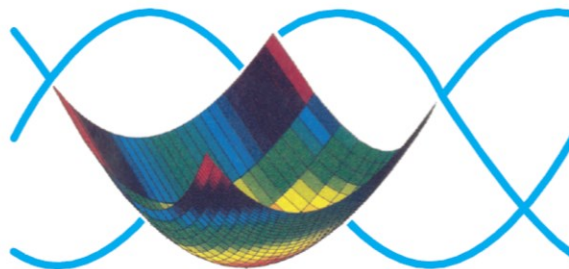


Valérie
Leprince
(INIVE, BE)

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5

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Experimental set-up and measurement of the Round
Robin Test Box at Plataforma Solar de Almeria
Overview of available data and analysis topics

María José JIMÉNEZ



6

CONTENTS



■ Introduction

- The role of simplified case studies to develop skills and methodologies

■ Round Robin Test Box

- Building
- Experiment set up
- Data

■ Data analysis topics

- Qualitative data analysis and pre-processing
- Constructing models from measured data and building physics



7

7

Case study: Round robin test box



- A **simplified building** has been considered as a case study.

- Round robin test box Annex 58

- Its **detailed and accurate knowledge** reinforces and complements the validation criteria.

- The robustness of the method can be analysed by comparing the results from a **long testing period** including different test and weather conditions.

- **Benchmark data and set-up**



8

8



INTRODUCTION (CONTEXT)



- **Dynamic models allows getting characteristic (steady state and others) parameters from **dynamic** tests campaigns**
 - Key feature for energy performance assessment of “as built” buildings, under **dynamic** outdoors weather and in-use conditions.
- **Key distinctive aspects of these “real life” tests conditions:**
 - **Time varying measurements**, calls for the application of system identification techniques and time series analysis tools.
 - **Many other physical phenomena** in these tests which are not present in other tests such as well controlled tests in laboratories and steady state.
- **Role of simplifications to get accurate results and design cost effective tests**



INTRODUCTION (CONTEXT)



- **Dynamic test conditions versus constant KPIs (parameters)**
 - KPIs can be can be constant parameters (intrinsic) or time varying
- **Dynamic analysis must be robust:**
 - Giving stable estimates for constant parameters
 - Allowing identifying dependencies for non constant indicators



Usefulness of well known simple systems




- Simplicity in the test component **doesn't mean simple** analysis
 - **Dynamic features** are still present
 - Complex **physical phenomena** occur
- Simplicity in the component allows us to put the **focus on**
 - The different analysis approaches highlighting the **main steps**
 - Dynamic features and other observable complex physical **phenomena that occur**
- Additional **validation criteria**: previous knowledge about thermal characteristics
 - External validity
- Well known characteristics facilitate to **identify wrong** results and check **analysis skills**




Usefulness of well known simple systems




- Facilitate detection of models that in principle could be considered **good candidates** but can give **wrong results**, even for a so simple case study
- Skills in **validation** strategies and techniques, play an important role in the process of detecting and rejecting wrong results
- Simplicity is very useful to develop awareness regarding the relevance of validation. It helps also to acquire **skills** in identifying and avoid mistakes that lead to wrong results



Usefulness of a wide variety of data series



- Useful support to validation
- Optimum and not optimum data series are useful to explore the accuracy of the applied approaches for different not optimum test conditions




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13


13



CONTENTS



- Introduction
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14

14

Case study

Round robin test experiment. IEA EBC annex 58

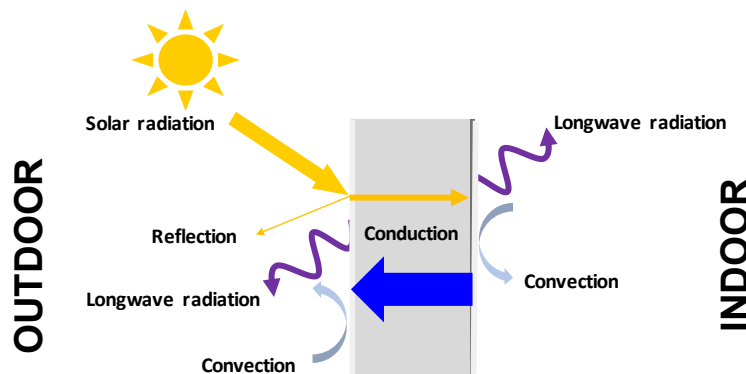
- Comparative experiment on testing and data analysis
- Scale model of a simplified building
- Tested by different partners: Different weather and measurement devices

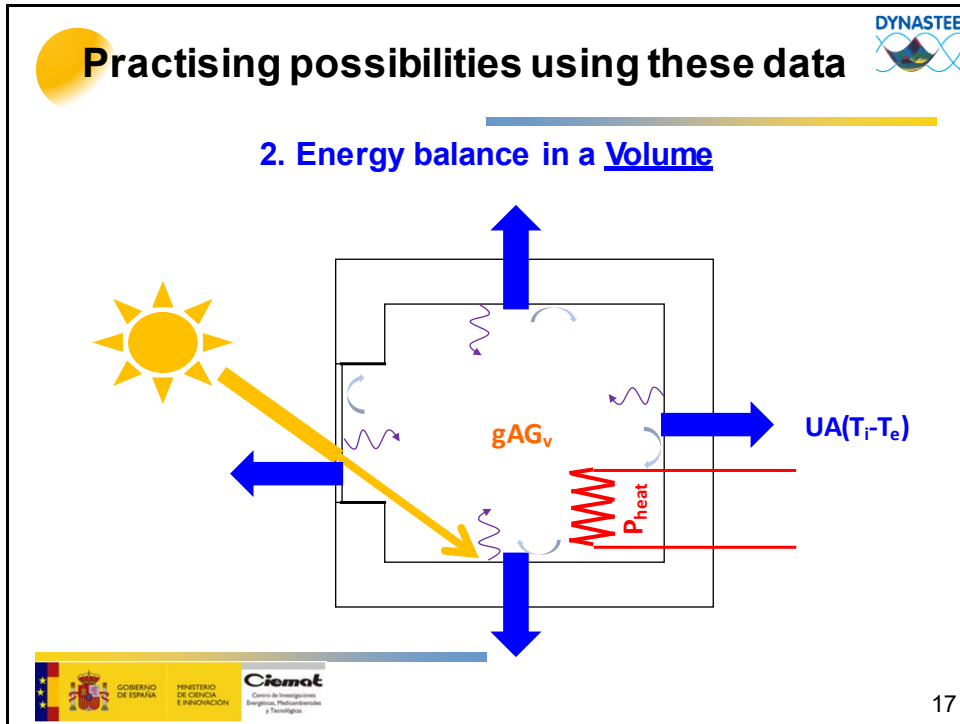


Case study

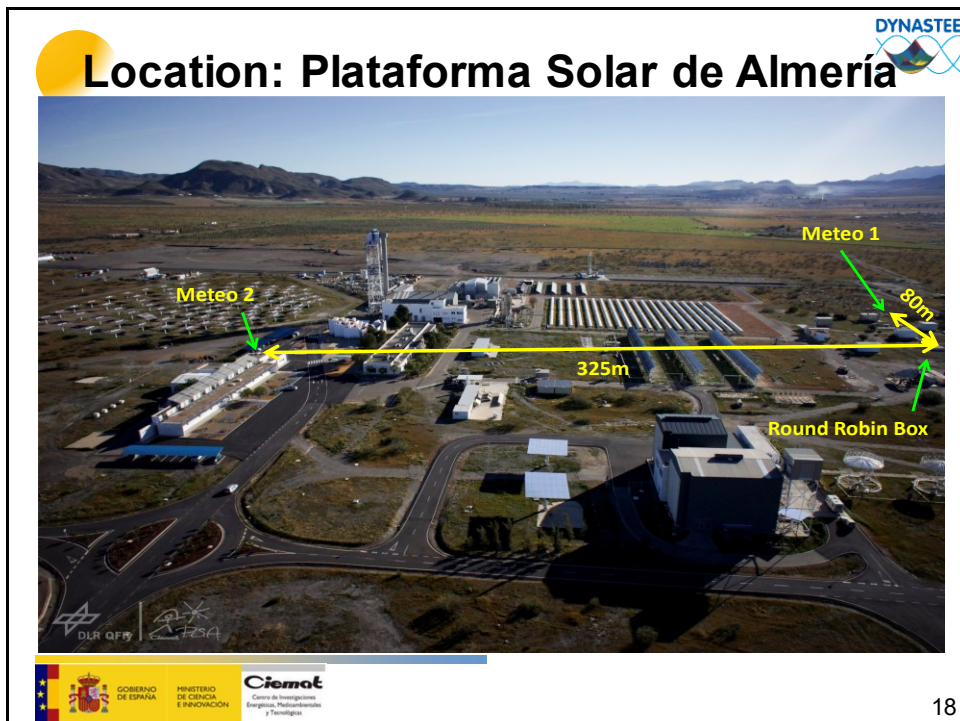
Practising possibilities using these data

1. Energy balance in a Surface





17



18

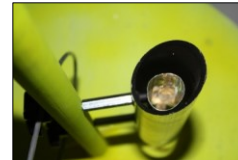
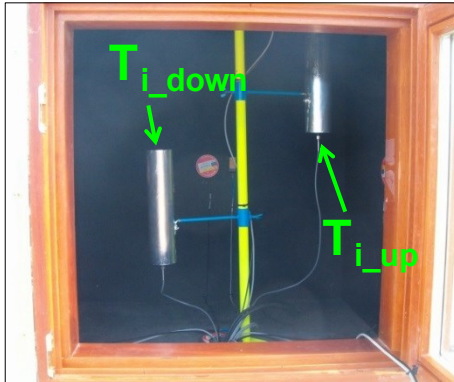
Measurement devices



Measurement devices



Air temperature: Sensor must measure the air temperature. How ?

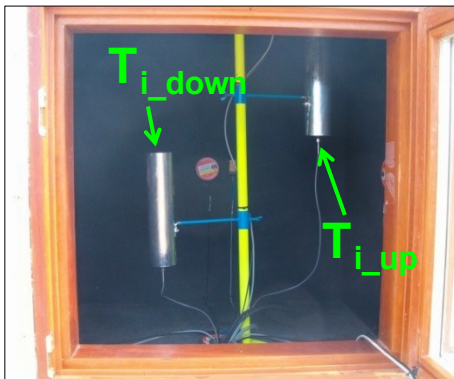


Indoor air temperature:
Sensor protected from solar radiation by aluminium cylinders that allow ventilation

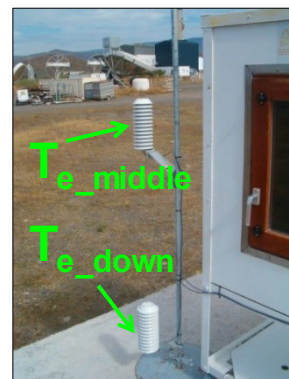
Measurement devices



Air temperature: Sensor must measure the air temperature. How ?



Indoor air temperature:
Sensor protected from solar radiation by aluminium cylinders that allow ventilation



Outdoor air temperature:
Shielded and ventilated devices
Natural ventilation driven by solar radiation
Solar radiation increases ventilation effect

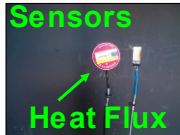
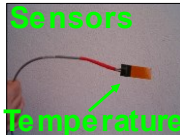
Measurement devices



Surface temperature: Sensor must measure the surface temperature

Heat flux through a surface: Sensor must measure the heat flux through the surface

How ?



Requisites:

The sensor must behave identically to the measured surface

- The sensors must be well integrated in the surfaces
- Contact between sensor and surface must be guaranteed
- Sensor surface must have the same optical properties as the measured surface

Implementation:

Glowing sensor to surfaces.

Painting the sensor with the same colour of the measured surfaces

Or protecting the sensor with adhesive tape with the same colour of the surface



23

23

Requisites to tests campaigns for analysis



- The experiment design must guarantee that the phenomena to be characterised are happening and strong enough for their analysis. A phenomenon is strong enough, when the amplitude of the corresponding driving variable is significantly higher than the uncertainty in its measurement. Otherwise signal to noise is poor.
- **Identification of heat transfer coefficient to the outdoors**, requires strong enough heat loss through the building envelope. Achieved **maximising the indoor to outdoor air temperature difference**, which is the driving variable in this case.
- **To identify the overall gA-value**, requires strong enough solar gains. Achieved when the experiment contains sunny days, when **solar radiation is high**, which is the driving variable in this case.
- **To identify the effective heat capacity** the system must be excited by **dynamic input signals** in a wide range of frequencies covering the characteristic time constants of the system.
- A good representation of indoor air temperature is necessary which requires **homogeneity**.



24

24

Data series



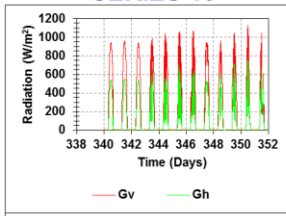
- **Series 16:** Since 06/12/2013, 12 days. With a ROLBS power sequence. Designed to optimise the test for the system identifications techniques.
- **Series 17:** Since 18/12/2013 9 days. Coheating test, but setting the indoor air temperature set point to 35°C. Designed to have a reference analysis, also to explore the application of steady-state approaches and to analyse the capability to apply the system identification techniques to this type of tests. Also useful to analyse causality issues and different variables as input signal
- **Series 18:** Since 27/12/2013, 12 days: Aiming to reproduce as possible a Coheating test, but setting the indoor air temperature set point to 21°C. More realistic conditions (close to comfort) to explore the possibilities to apply the identification techniques to in-use buildings and on board monitoring systems. Also interesting to analyse causality issues and different variables as output signal. Increased difficulty: Low ΔT and correlation of T_i to solar radiation.
- **Other data available:** 9-month test campaign with other test and boundary conditions. Other seasons, infiltrations, different orientations or including PCM.



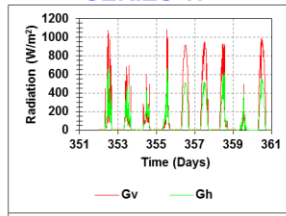
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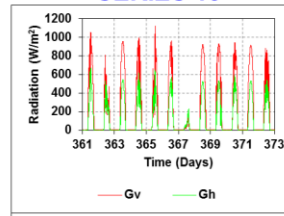
SERIES 16



SERIES 17

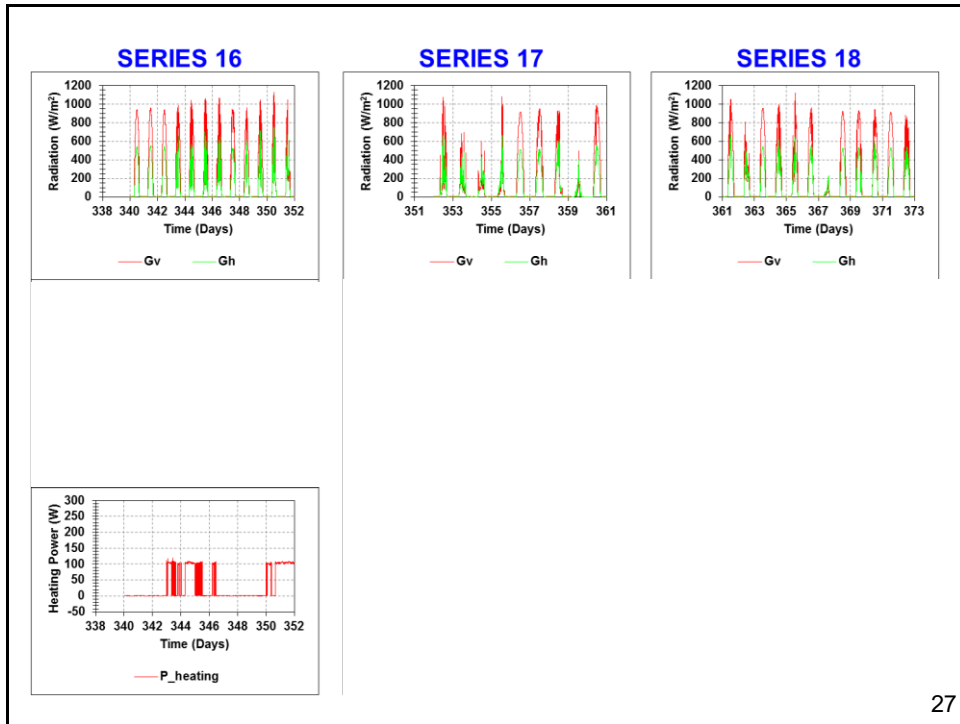


SERIES 18



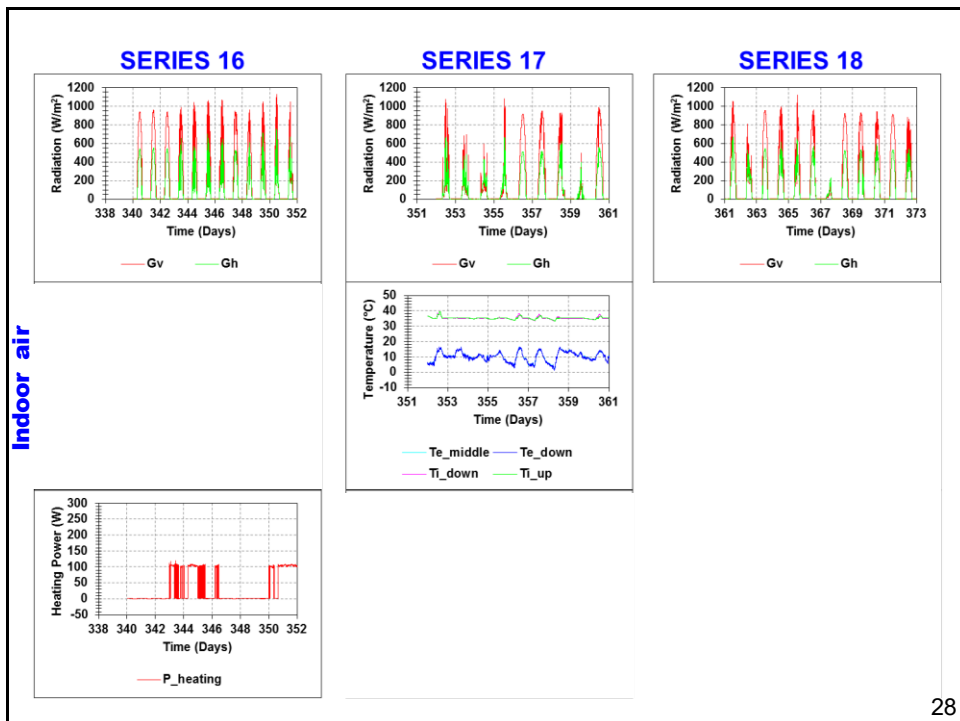
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26



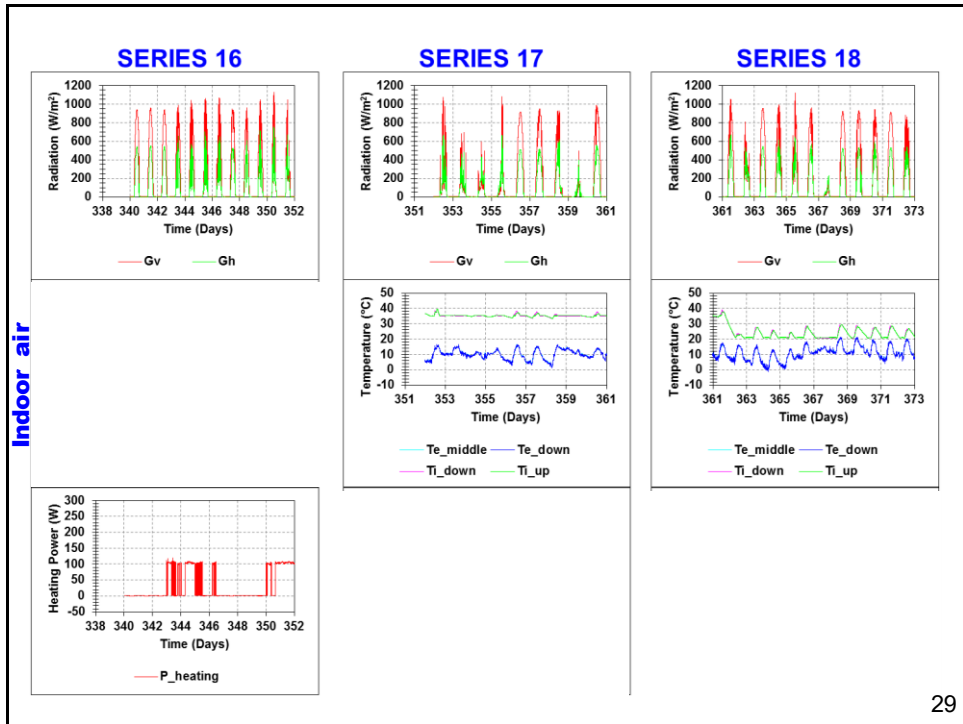
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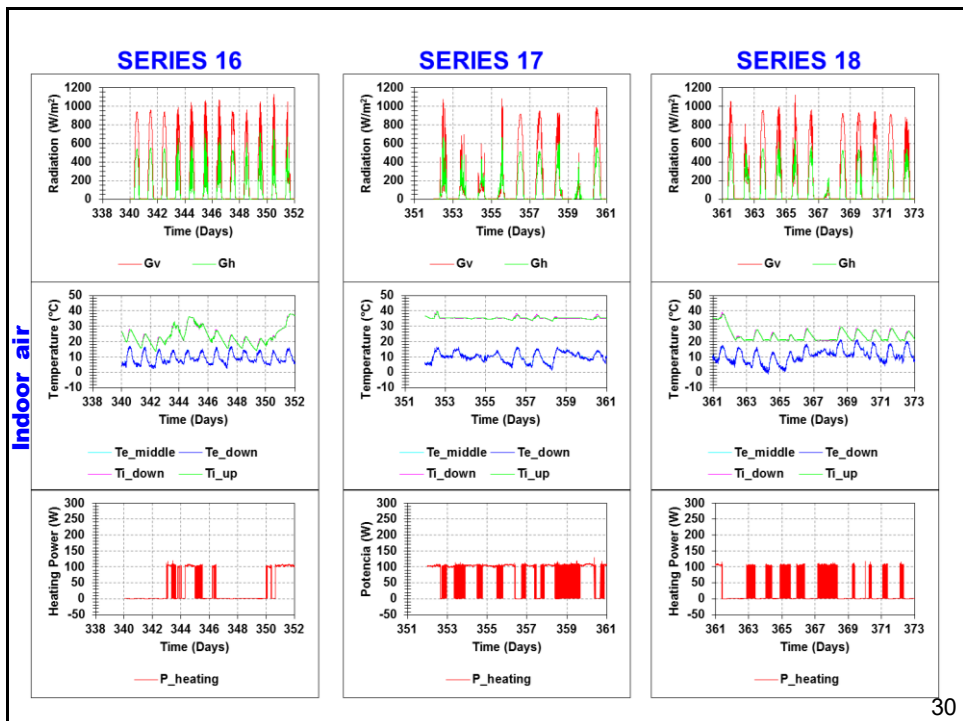
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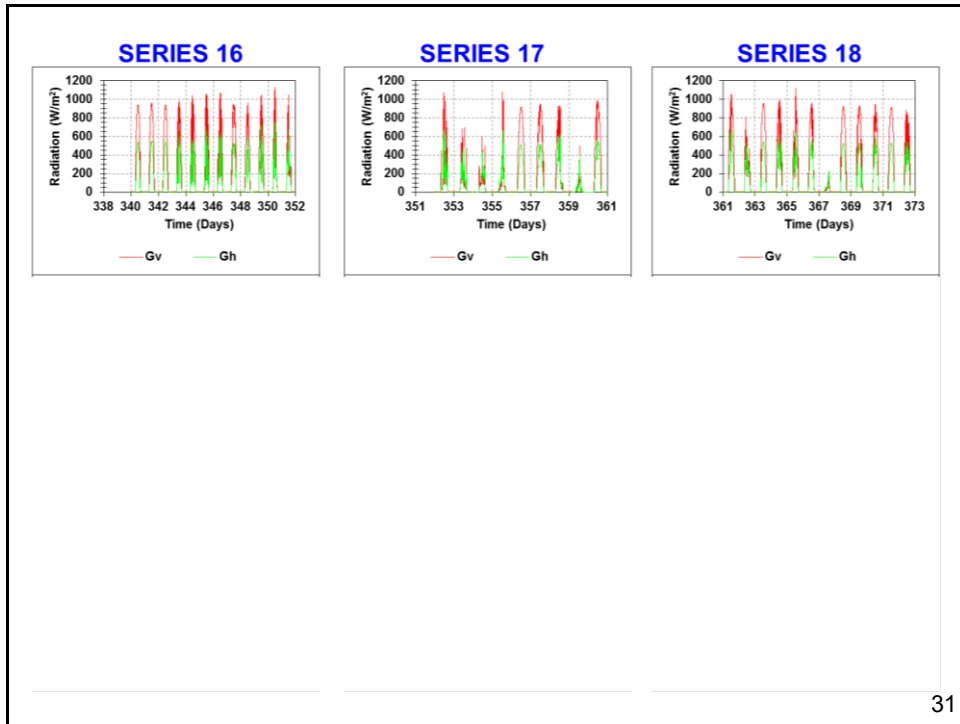
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29



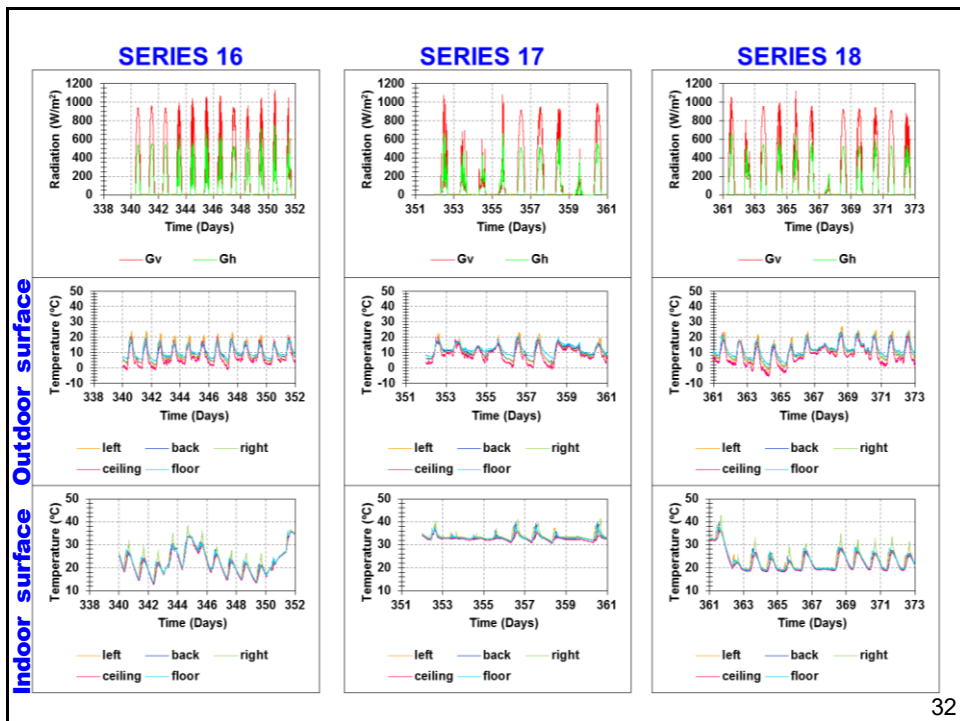
30

30



31

31



32

32



CONTENTS



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33

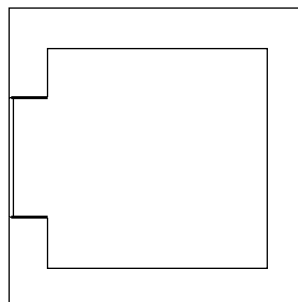
33



Candidate models including and not including solar gains through opaque walls.



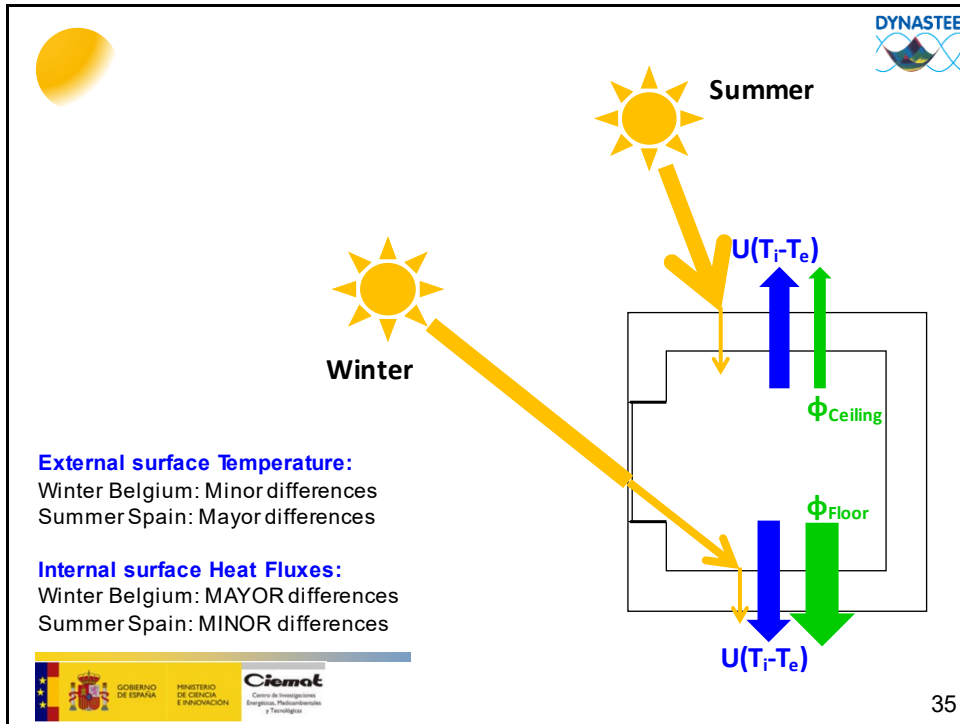
Do they make sense?



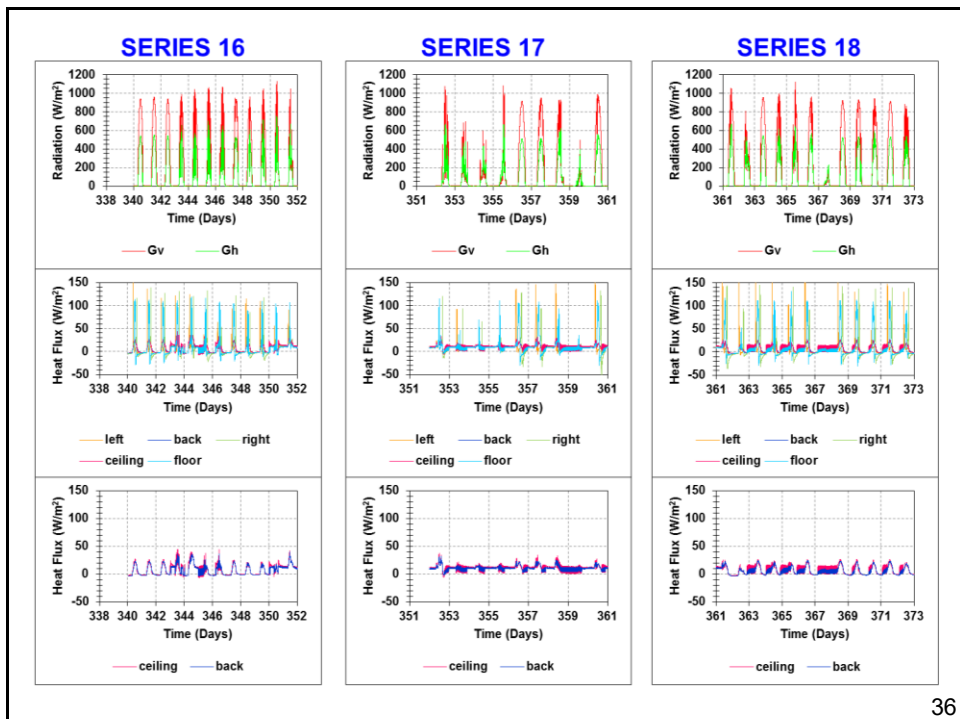
Yes taking into account next slides.....

34

34



35



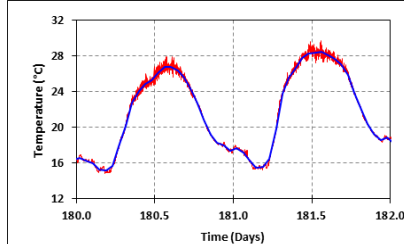
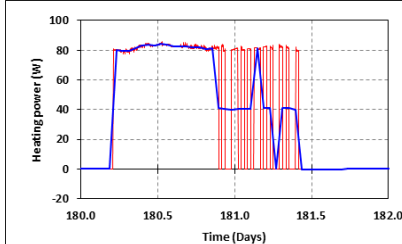
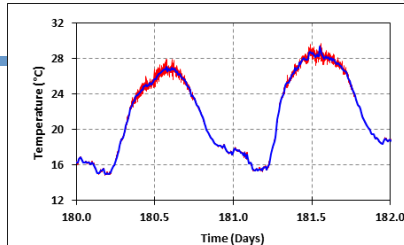
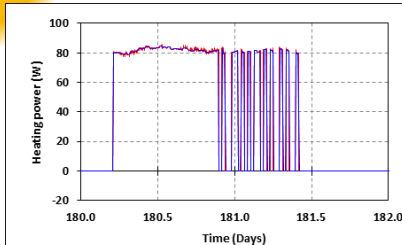
36

Pre-processing, Averaging, Filtering

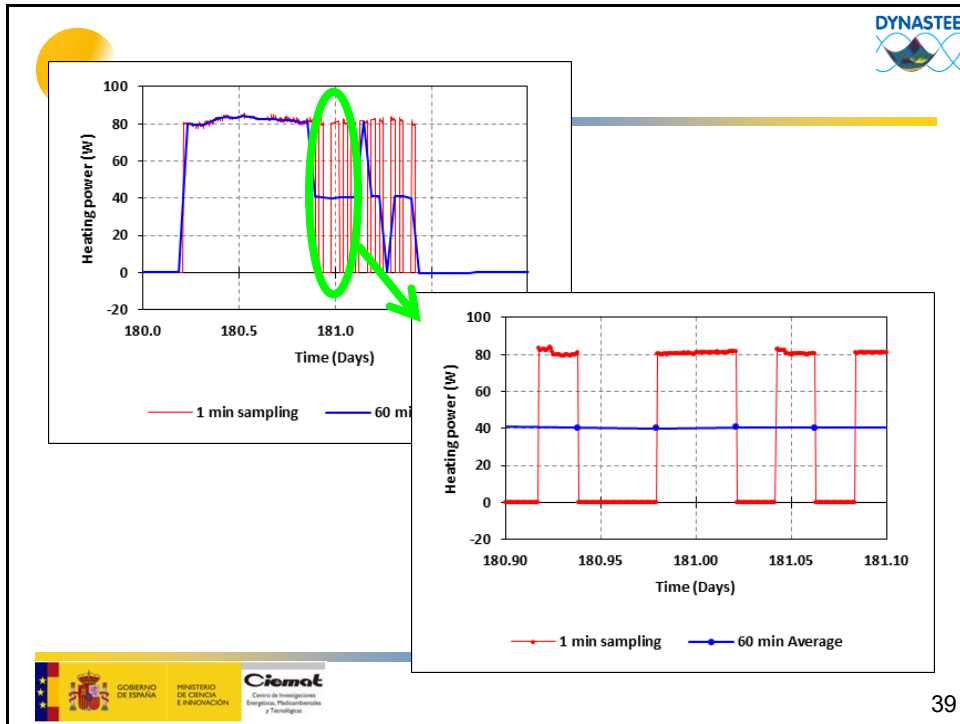


- Data analysis starts with **qualitative analysis** of data based on data overview, aiming to detect any abnormal behavior in the tendencies of variables, sensor failures, etc.
- Filtering techniques are **useful when** there is certainty that removed **information doesn't correspond to the phenomena** that we want to study
- Filtering and averaging could have **harmful effects if it removes relevant information** to the process under study (See aliasing in statistical guidelines)
- If averaging or filtering are applied they must be justified: what does it mean? which are the expected benefits?, why improvements are expected?, etc.

37



38



39

METHODS FOR DATA ANALYSIS: SUMMARY

- **STEADY STATE**
 - Average method, linear regression...
- **DYNAMIC APPROACHES**
 - Linear models in transfer function form
 - ➔ ARX, ARMAX
 - State space models
 - ➔ RC, SDE

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40



Construction of candidate models



Based on physical knowledge

- Starting point is an **energy balance equation including**:
 - the characteristic (usually intrinsic) **parameters that must be identified**
 - the **time recorded variables** driving the main heat fluxes of the system.
- The characteristics of the studied component and given test conditions are taken into account to build all the candidate models in **all the applied approaches**.
- It is important to be aware that all these considerations must be taken into account also to define the specifications of experiment set up.



Construction of candidate models



HYPOTHESES DERIVED FROM PHYSICAL KNOWLEDGE OF THE SYSTEM

Candidate models must be written trying to give answer to the following questions

- What is the **system** to which the energy balance equation will be referred to?. Is a volume?, is a flat surface?
- What are the **phenomena theoretically** in the energy balance equation?
- Which of these **phenomena are relevant** in practice to the considered case study and given test conditions?
- What is the most **efficient way of modelling** each relevant phenomena?. Efficiency is referred to model accuracy, cost of measurement devices, and model simplicity.
- Which are the **main driving variables** of each of the phenomena recognised as relevant for the considered case study?
- Which variables must be considered inputs and outputs according to **causality**.

If it is not possible to answer some of these questions a priori, **several candidate models** according to the different possibilities can be considered and evaluated.

Analysis approaches applied and key issues common to all the analysis approaches

- Analysis to obtain the HLC of the whole building based on the ENERGY BALANCE EQUATION IN THE AIR VOLUME confined by the house envelope
- Analysis to obtain the U of the opaque walls based on the ENERGY BALANCE EQUATION IN THEIR INTERIOR SURFACE
- First step: check the **availability and quality of the driving variables** of the terms required to write candidate models based on this energy balance.
- Data: Several data set used to check robustness and replicability of results
- Common principles to different **approaches**:
 - **RC Models** Identified using LORD, (or CTSM-R)
 - **Linear regression**
 - **ARX Models** Identified with MATLAB IDENT
 - Etc.

43

43

Analysis approaches applied and key issues common to all the analysis approaches

- Analysis to obtain the HLC of the whole building based on the ENERGY BALANCE EQUATION IN THE AIR VOLUME confined by the house envelope
- Analysis to obtain the U of the opaque walls based on the ENERGY BALANCE EQUATION IN THEIR INTERIOR SURFACE
- First step: check the **availability and quality of the driving variables** of the terms required to write candidate models based on this energy balance.
 - Heat lost to outdoor
 - Solar gains
 - Heat supplied by heating system (to obtain HLC) or Heat Flux (to obtain U)
 - Other contributions that could be present in other real life cases: Internal gains due to appliances, Heat removed by the mechanical ventilation system, Heat exchanged with adjacent houses, Heat supplied due to metabolic activity

44

44

**Key issues common to all the analysis approaches:
Modelling energy contributions to the energy balance**

ENERGY BALANCE TERM → DRIVING VARIABLES

- | | |
|--|---|
| ■ Heat lost to outdoor | ■ $T_{\text{indoor}} - T_{\text{outdoor}}$ |
| ■ Solar gains | ■ On site solar radiation |
| ■ Internal gains due to appliances | ■ Total electricity consumption |
| ■ Heat removed by the mechanical ventilation | ■ Air flow, and supply and return temp |
| ■ Heat supplied by the heating system | ■ Heating power |
| ■ Heat flux through the interior surface | ■ Heat flux through the interior surface |
| ■ Heat exchanged with adjacent houses (j) | ■ $T_{\text{indoor}_1} - T_{\text{indoor}_j}$ |
| ■ Heat supplied due to metabolic activity | ■ ? (<i>Applied Energy</i> , 199, pp. 121–141) |

45

45

METHODS FOR DATA ANALYSIS: SUMMARY



■ STEADY STATE

- Average method, linear regression...

■ DYNAMIC APPROACHES

- Linear models in transfer function form
 - ➔ ARX, ARMAX
- State space models
 - ➔ RC, SDE

46

46

RC MODELS



- Electrical analogy, with energy balance referred to a node of the system.
- Justified translation from thermal system to electrical scheme is required
- **Typical aspects** that require considering different candidate models
 - Different **number of resistances** in series (different number of nodes) are recommended for systems with **un-known heat capacity**
 - Evaluation of **solar radiation transmitted through opaque walls**: Is or isn't relevant (absorbed during the day in the walls and released to outdoors at night and don't reach indoors)?
 - **Parallel branches** representing building envelope with low mass glassing elements and heavier opaque walls
 - Symmetry can be assumed to avoid over-parameterisation
- **Any other relevant contribution to the energy balance must be represented**



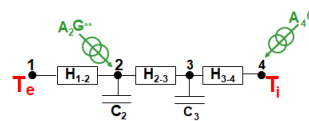
47

47

RC Models Identified with LORD. Possibilities

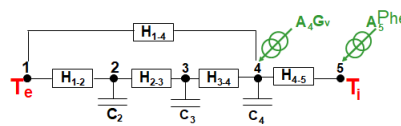
1. Mono-dimensional analysis of opaque walls

- To obtain the U value of the opaque walls
- Several candidate models. Relevant options:
 - 3 to 7 nodes
 - Outputs: T_i , ϕ
 - Including and non-including solar radiation
 - Systematic analysis of the ceiling considering all the options
 - Analysis of floor and left, right, back walls using best model found for the ceiling



2. Tri-dimensional analysis of the whole building

- To obtain the UA and gA values of the whole building envelope
- Several candidate models. Relevant options:
 - 3 to 7 nodes representing opaque walls
 - Parallel branch representing the window
 - Outputs: T_{ii} , $P_{heating}$
 - All candidate models including G_v
 - Evaluation of best model found for the considering non-measured variables



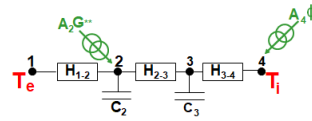
48

48

RC Models Identified with LORD. Possibilities

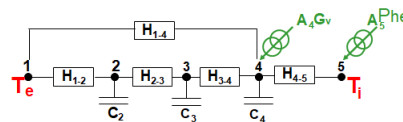
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2. Tri-dimensional analysis of the whole building

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- Several candidate models. Relevant options:
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 - Parallel branch representing the window
 - Outputs: T_i, P_{heating}
 - All candidate models including G_v



49

49


STEADY STATE ANALYSIS




- **Steady state test:** all physical quantities are time independent (ISO 9251:1987).
- **Steady state equations**
 - Steady state equations **based on instantaneous measurements are not valid** for dynamic tests
- **Integrated dynamic** equations are analogous to **steady state** equations.
 - Using time averaging to represent integrals
 - Steady state equations **based on averages can lead to accurate results** for dynamic tests under certain conditions
 - **Many drawbacks: Usually require extremely long test periods, etc.**

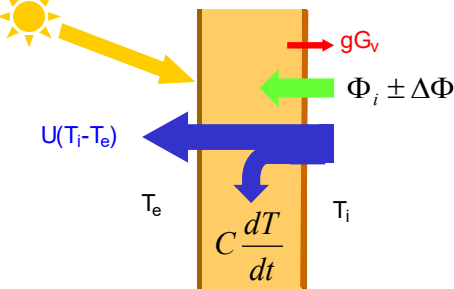
50

50



METHODS BASED ON AVERAGES. SEEN AS DYNAMIC INTEGRATED APPROACHES





$\Phi_i = C \frac{dT}{dt} + U(T_i - T_e)$

Considering:

- Integrals for long periods, Δt
- Integration period **long enough** to :

$$\int_i^\Delta C \frac{dT}{dt} dt \ll \int_i^\Delta \Phi_i dt - \int_i^\Delta U(T_i - T_e) dt$$

- Averages to estimate integrals:

$$0 \cong \overline{\Phi_i} - U(\overline{T_i} - \overline{T_e})$$


Generalisation

$$\overline{y} = a_1 \overline{x_1} + a_2 \overline{x_2} + \dots + a_n \overline{x_n} + b$$


- Wind speed, solar radiation, long wave radiation?
- If their influence on Φ , is higher than $\Delta \Phi$. Depend on the component and weather.
- Other effects, other systems

NO


YES


51

51



Published papers relevant to this method




K. Chávez, D.P. Ruiz, M.J. Jiménez. 2019. Dynamic integrated method applied to assessing the in-situ thermal performance of walls and whole buildings. Robustness analysis supported by a benchmark set-up. *Applied Thermal Engineering*. **152C**, pp. 287-307. DOI: [10.1016/j.applthermaleng.2019.02.065](https://doi.org/10.1016/j.applthermaleng.2019.02.065)

J.A. Díaz, M.J. Jiménez. 2017. Experimental assessment of room occupancy patterns in an office building. Comparison of different approaches based on CO₂ concentrations and computer power consumption. *Applied Energy*. **199**, pp. 121–141. DOI: [10.1016/j.apenergy.2017.04.082](https://doi.org/10.1016/j.apenergy.2017.04.082)

L. Castillo, R. Enríquez, M.J. Jiménez, M.R. Heras. 2014. “Dynamic integrated method based on regression and averages, applied to estimate the thermal parameters of a room in an occupied office building in Madrid”. *Energy and Buildings*. **81**, pp. 337-362. DOI: [10.1016/j.enbuild.2014.06.039](https://doi.org/10.1016/j.enbuild.2014.06.039)

I. Naveros, M.J. Jiménez, M.R. Heras. 2012. “Analysis of capabilities and limitations of the regression method based in averages, applied to the estimation of the U value of building component tested in Mediterranean weather”. *Energy and Buildings*. **55**, pp. 854-872. DOI: [10.1016/j.enbuild.2012.09.028](https://doi.org/10.1016/j.enbuild.2012.09.028)


52

52



TRANSFER FUNCTION FORM (ARX, etc)



- Output is linear function of a number of past readings of the inputs and outputs
- Physical parameters found comparing equations that must coincide:
 - The steady-state energy balance equation
 - The ARX model, when all its inputs and outputs are constant.
- ARX model **MUST** contain the same variables as a steady state energy balance eq.
 - Key step in this approach is to deduce and write the appropriate steady state energy balance equation that must be based on physical knowledge.
- Different candidate models based on different assumptions and approximations
- Assignment of inputs and outputs based on causality



Published papers relevant to this method



- Jiménez M.J., Madsen H., Andersen K.K. 2008. Identification of the Main Thermal Characteristics of Building Components using MATLAB. *Building and Environment*. 43(2), pp. 170-180. DOI: [10.1016/j.buildenv.2006.10.030](https://doi.org/10.1016/j.buildenv.2006.10.030)
- Jiménez M.J., Madsen H., Andersen K.K., "How to get physical parameters using MATLAB". Presented at "International Conference on Dynamic Analysis and Modelling Techniques". Organised by PASLINK EEIG and JRC. Ispra. (Italy). 13-14 November 2003. ISBN 92-894-7794-6. Paper in the DYNASTEE USB: [\Ispra2003PapersPDF\p129_Jimenez.pdf](#)
- Jiménez M.J.; Heras M.R. 2005. "Application of multi-output ARX models to estimate the U and g values of building components from outdoors testing". *Solar Energy*. 79(3), pp. 302-310. DOI: [10.1016/j.solener.2004.10.008](https://doi.org/10.1016/j.solener.2004.10.008)
- M.J. Jiménez, B. Porcar, M.R. Heras. 2008. "Estimation of UA and gA values of building components from outdoor tests in warm and moderate weather conditions". *Solar Energy*. 82(7), pp. 573-587. DOI: [10.1016/j.solener.2008.02.013](https://doi.org/10.1016/j.solener.2008.02.013)



STOCHASTIC STATE SPACE MODELS



- Very useful and flexible to represent physical systems governed by differential eq.
 - Offers a very high potential to model a wide variety of physical systems
- Diffusion terms and modelling errors facilitate very accurate parameter estimates
- System equations can include measured as well as non-measured states
 - Which is a very useful in modelling physical systems
- RC models can be considered. This family of models:
 - Are a reduced subset of the state space models than can be used
 - Don't make use of these capabilities in their full extent



Published papers relevant to this method



- M.J. Jiménez, H. Madsen, H. Bloem, B. Dammann. 2008. "Estimation of Non-linear Continuous Time Models for the Heat Exchange Dynamics of Building Integrated Photovoltaic modules". Energy and Buildings. 40(2), pp. 157-167. DOI: [10.1016/j.enbuild.2007.02.026](https://doi.org/10.1016/j.enbuild.2007.02.026)
- N. Friling, M.J. Jiménez, J.J. Bloem, H. Madsen. 2009. "Modelling the heat dynamics of building integrated and ventilated photovoltaic modules". Energy and Buildings. 41(10), pp. 1051-1057. DOI: [10.1016/j.enbuild.2009.05.018](https://doi.org/10.1016/j.enbuild.2009.05.018)
- Jiménez M.J., Madsen H. 2008. "Models for Describing the Thermal Characteristics of Building Components". Número especial sobre ensayos de cerramientos en condiciones reales. Building and Environment. 43(2), pp. 152-162. DOI: [10.1016/j.buildenv.2006.10.029](https://doi.org/10.1016/j.buildenv.2006.10.029)

Model validation



- **Fit to the data.** The model residuals should be 'small' and 'white noise'.
- **Internal validity.** The model should agree with data other than data used for parameter estimation (cross validation)
- **External validity.** The result from the model should not (without greater motivation) conflict with previous experiences or other known conditions.
- **Dynamic stability.** From a steady state, the model should give an output upon a temporary change in an input variable that is gradually faded out (if the model is intended to describe dynamic characteristics).
- **Identifiability.** It should be possible to determine the parameters of the model uniquely from the data
- **Simplicity.** The model should be as small as possible

U. Norén. 1994. In:

Workshop on Application of System Identification In Energy Savings In Buildings



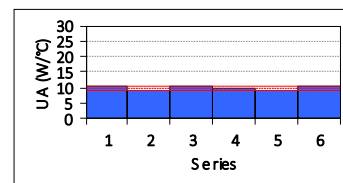
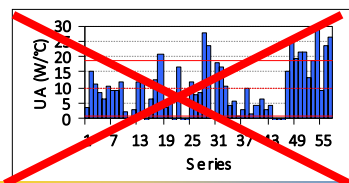
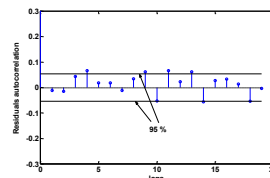
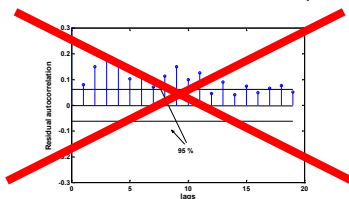
57

57

Model validation



- **Mandatory**
- **Statistical** criteria are very useful in the process of model selection
- Results must not contradict **physical knowledge** and common sense
- If validation criteria are not fit, results must be rejected and models reformulated



58

58



Interpretation of residuals



- **Residuals with a frequency of 24 hours** very frequent in insufficient models
- Non negligible correlation between model residuals and solar radiation, could inspire more **detailed description of the solar radiation** to improve model.
- **Sometimes better modelling solar radiation is not a solution:** Many variables can have relevant correlation with solar radiation, so **any other effect** depending on them and not properly modelled **can show residuals in the same frequency**.



Interpretation of residuals



- Many variables can have relevant correlation with solar radiation, so **any other effect** depending on them and not properly modelled **can show residuals in the same frequency**. Examples:
 - **Air leakage** that can depend on wind speed and/or outdoor air temperature, both depending on solar radiation
 - **Longwave effects** stressed by high surface temperatures due to solar radiation
 - U depending on **thermal conductivities** depending on temperature of materials that depends on solar radiation
 - **Wrong resampling** disregarding the sampling theorem



Frequent mistakes in model building



- Use equation from literature that include approximation under strong hypotheses that doesn't fit the particular studied problem
- Use excessively detailed equations when some their terms are in practice negligible, bringing too many variables some of them supplying exclusively noise instead of information
- Ignore causality issues
- Ignore some aspects of reality of sensors
- Interpretation of problems in the residuals analysis in the frequency of 24 hours
- Eliminate from energy balance equations constant inputs



Recommended reference



Chapter 11 of: IEA, EBC Annex 58, Report of Subtask 3, part 1. Thermal performance characterization based on full scale testing - description of the common exercises and **physical guidelines**

[Link to the full document](#)

[Link to physical guidelines](#)

[Link to PSA_RRbox_DataSeries20.zip](#)



Thank you for the attention



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e-mail: mjose.jimenez@psa.es

Introduction to LORD

Dr Paul Baker

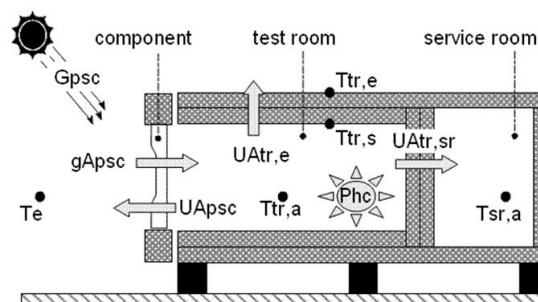
Building Physics Consultant



1

Origins

- LORD was developed for the PASLINK EEIG by Olaf Gutschker, BTU Cottbus, to analyse **dynamic test cell data** and deliver high quality performance characteristics for building components tested in real climates.



SS21

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Purpose

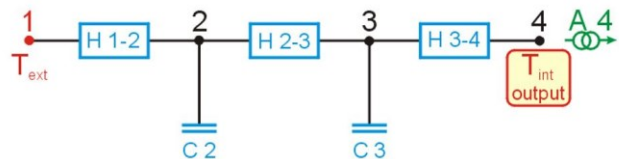
- LORD can be used for components (walls, windows etc), whole rooms or more complicated systems;
- to obtain **thermal transmittance values**, **solar gain factors**, and possibly dynamic information (e.g. capacitances, time constants).
- A transient mathematical model is assumed. The parameters of the model (e.g. resistances, capacitances and heat flow admittances) essentially define the dynamic and steady-state thermal and solar properties of the system.

SS21

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3

The user defines a RC-network



- Initial guesses of the parameter values are made.
- The **output** of the actual test (for instance, the test room temperature T_{int} as a function of time) is compared with the **output** which the model produces for the same **input** conditions.
- By statistical analysis of the deviations between the model and the measured outputs, the parameter values are progressively adjusted in order to improve the agreement.
- Read LORD Manual and other documents which will be provided.

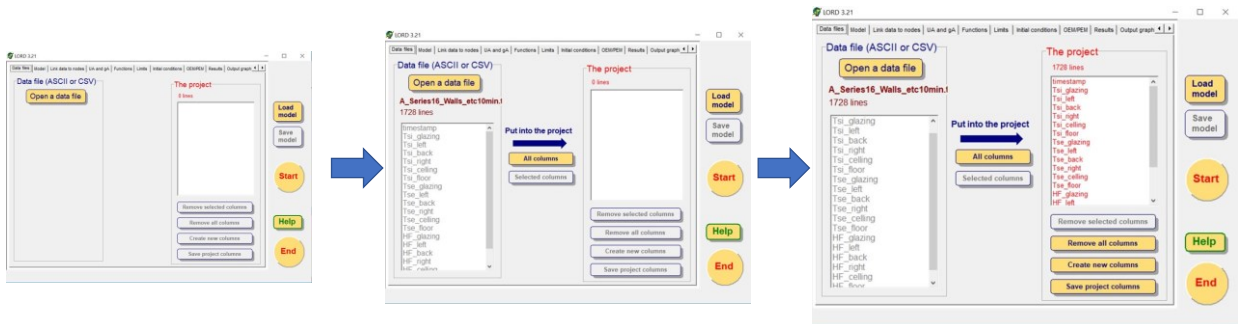
SS21

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(Mostly) User friendly interface

Step 1 - Input data: go to Data File tab.



SS21

5

5

File formats – tab delimited or CSV

Headers must be enclosed in single quotation marks

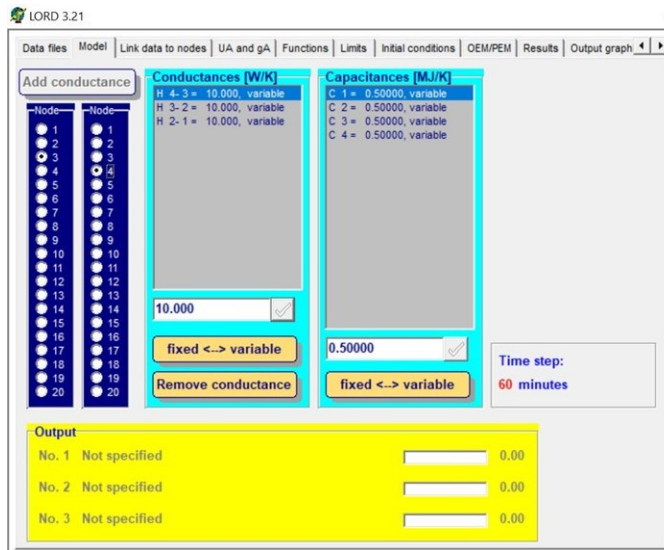
	A	B	C	D	E	F	G
1	'timestamp'	'Tsi_glazing'	'Tsi_left'	'Tsi_back'	'Tsi_right'	'Tsi_ceiling'	'Tsi_floor'
2	41614	22.7454834	26.606781	26.6628572	27.2989349	26.4609832	28.63676
3	41614.00694	22.5884704	26.4465637	26.4946289	27.1242904	26.2911529	28.49256
4	41614.01389	22.4506836	26.2751311	26.3376159	26.9624634	26.134137	28.34516
5	41614.02083	22.3161011	26.1245224	26.1822051	26.7862244	25.9658966	28.19936
6	41614.02778	22.1959381	25.9626922	26.0299851	26.6083832	25.7912597	28.04554
7	41614.03472	22.0549438	25.7896576	25.8681641	26.4337463	25.6230316	27.91416
8	41614.04167	21.9043121	25.6278382	25.7063447	26.263916	25.4532013	27.77157

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6

6

Step 2 – Create a model



Usually set capacitances at internal and external nodes to zero.



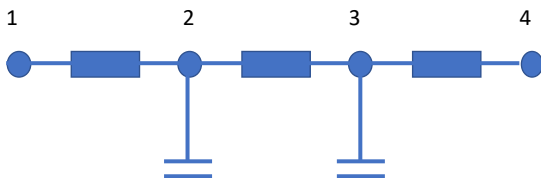
Check that time step is correct (note default is 60 minutes)



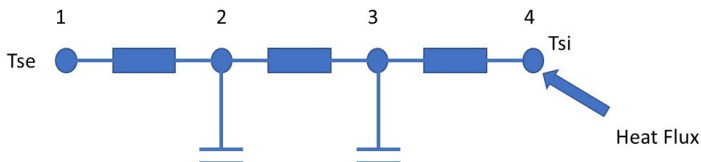
SS21

7

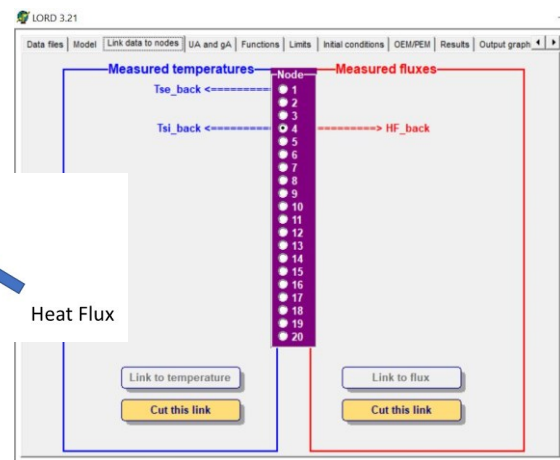
7



Step 3 – Link data to nodes



We now have a basic four node model which could be applied to heat flow measurements through a wall.



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8

8

Step 4 – Go back to Model!

Conductances [W/K]
 H 4-3 = 10.000, variable
 H 3-2 = 10.000, variable
 H 2-1 = 10.000, variable
 10.000

Capacitances [MJ/K]
 C 1 = 0, fixed
 C 2 = 0.50000, variable
 C 3 = 0.50000, variable
 C 4 = 0, fixed

Apertures
 A 4 = 1.0000, variable
 1.0000
 fixed <--> variable

Fix Aperture = 1
 for measured *Heat Flux* or
Heating Power

Apertures
 A 4 = 1.0000, fixed
 1.0000
 fixed <--> variable

Select Output

Output
 No. 1 Not specified 0.00
 No. 2 Not specified 0.00
 No. 3 Not specified 0.00

Output
 No. 1 Temperature "Tse_back" at node 1
 No. 2 Temperature "Tsi_back" at node 4
 No. 3 Flux "HF_back" at node 4

For *Solar Radiation* Aperture is
variable.

Output
 No. 1 Flux "HF_back" at node 4 1.00
 No. 2 Not specified 0.00
 No. 3 Not specified 0.00

SS21

9

9

Step 5 - UA & gA

Note for 1-D heat flux measurements = U- & g-values

For our 4-node model we need to specify interior & exterior nodes:

The UA- and the gA-value can be calculated automatically. For calculation of the UA-value, the interior node (e.g. the node associated with the interior air temperature) and the exterior node (e.g. the node associated with the ambient air temperature) must be specified. For calculation of the gA-value, additionally the column name of the solar radiation in the plane of the component must be specified.

Interior node: not specified
 Exterior node: not specified
 Vertical radiation: not specified

Select interior node
 Node number 1
 Node number 2
 Node number 3
 Node number 4
 none



The UA- and the gA-value can be calculated automatically. For calculation of the UA-value, the interior node (e.g. the node associated with the interior air temperature) and the exterior node (e.g. the node associated with the ambient air temperature) must be specified. For calculation of the gA-value, additionally the column name of the solar radiation in the plane of the component must be specified.

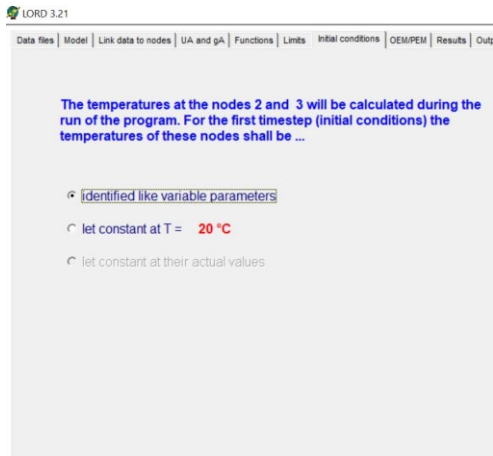
Interior node: Node number 4
 Exterior node: Node number 1
 Vertical radiation: not specified

SS21

10

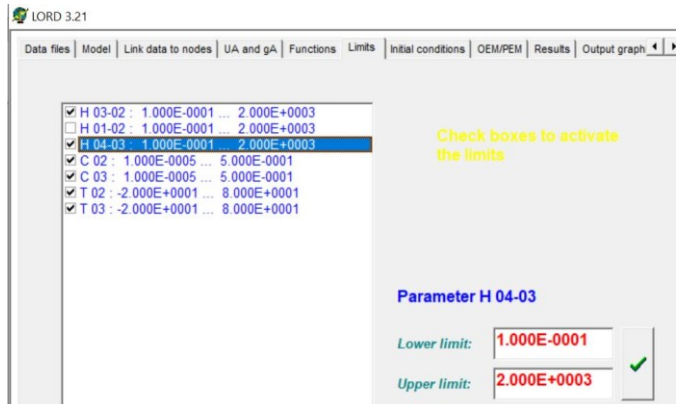
10

Step 6 – Initial Conditions



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Step 7 – Limits



11

11

Step 8 – OEM/PEM

Recommend



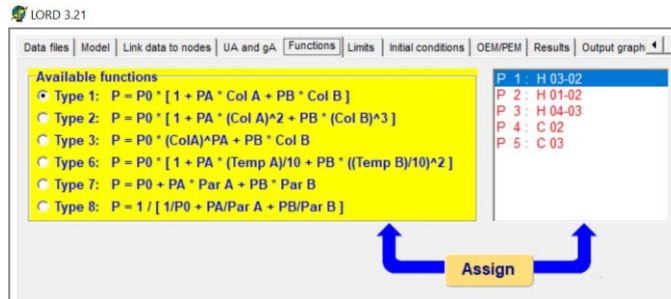
- LORD originally developed using OEM. PEM added later.
- In general, the residuals using PEM are smaller than using OEM.
- The identification process takes much longer using PEM.
- PEM can only be used if the outputs are measured temperatures.
- Ask a statistician to explain!

SS21

12

12

Other Options - Functions



For example, it is possible to create a variable resistance dependent on a measured parameter such as wind speed.

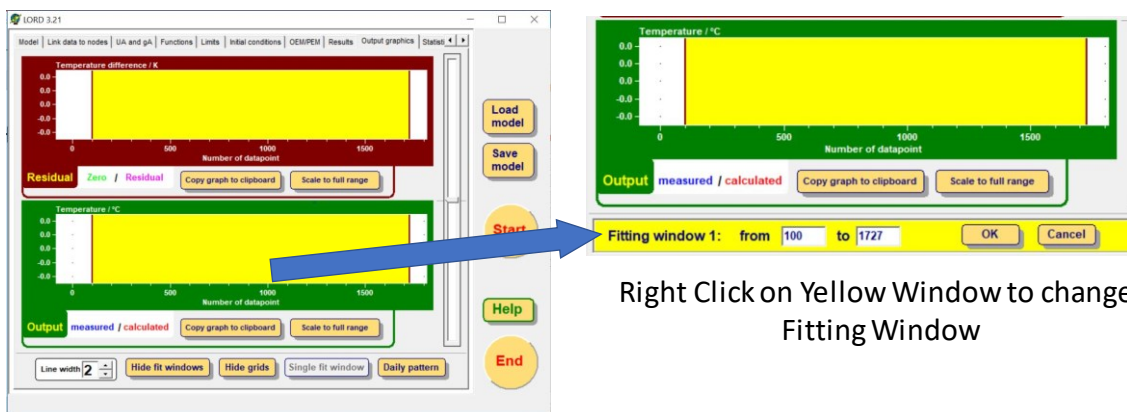
SS21

13

13

Other Options – Output Graphics & ‘Fitting Windows’

- Fitting windows can be used to select only part of the data for analysis.
- See LORD help for instructions.



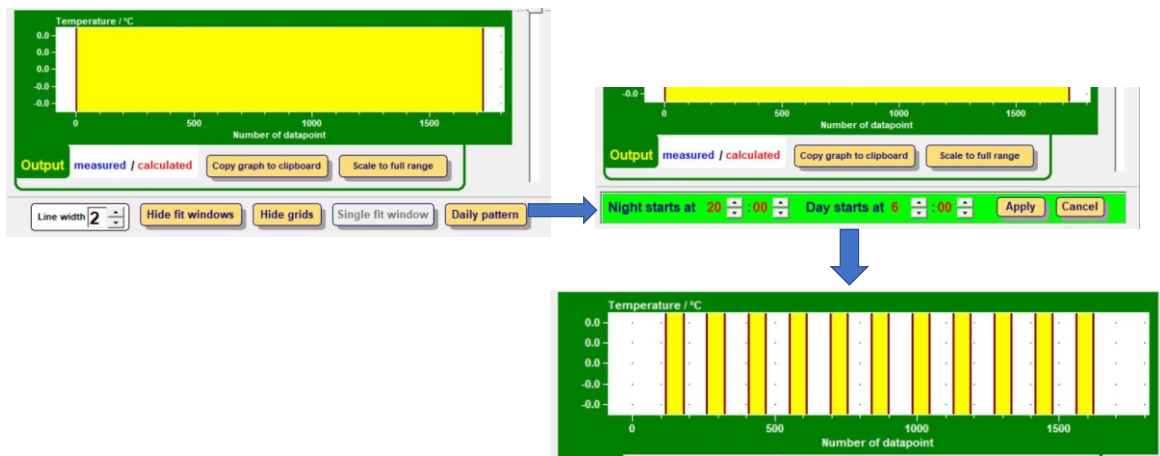
Right Click on Yellow Window to change Fitting Window

SS21

14

14

Daily Pattern – useful, for example, for excluding daytime data for heat flow measurements through windows.

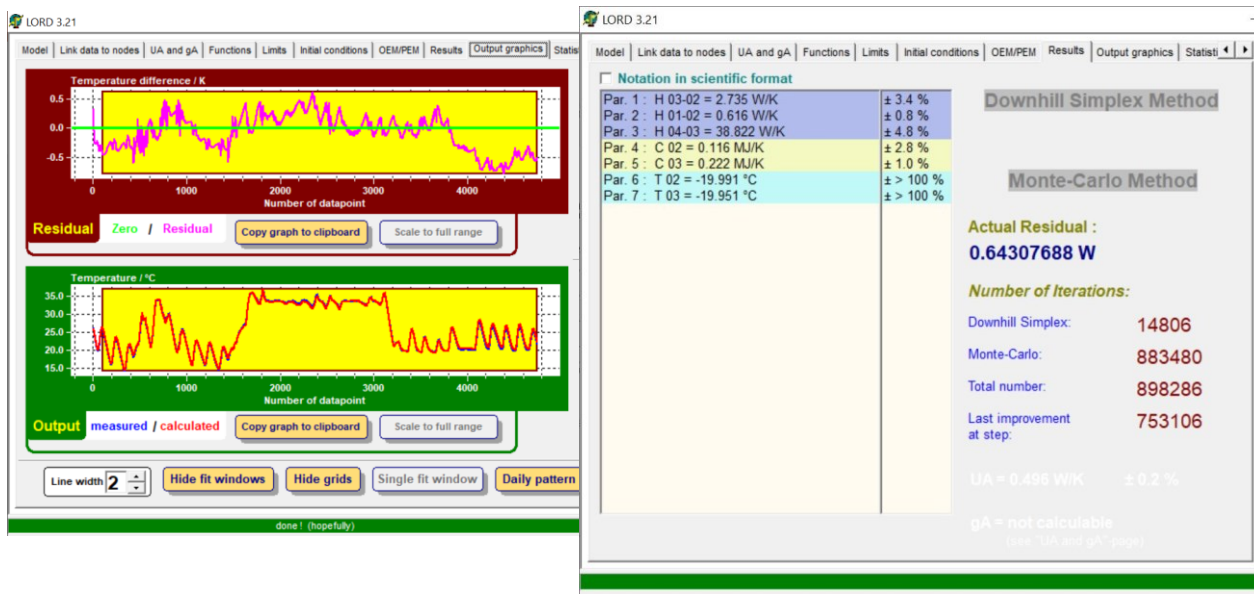


SS21

15

15

Run!



SS21

16

16

Results - Output File *.log gives all input and output information

```

Back_10min-5 - Notepad
File Edit Format View Help
Log-File, created by LORD
*****
Date: 17/06/2020
Time: 14:39:33
Time step: 10.00 minutes
Fitting window:
number 1 - from 180 to 4751
*****
Model and start values
*****
Conductances [W/K]
H 4-3 = 38.822, variable, limited between 0.10 and 2000.00
H 3-2 = 2.7932, variable, limited between 0.10 and 2000.00
H 2-1 = 0.65059, variable
*****
Capacitances [MJ/K]
C 1 = 0, fixed
C 2 = 0.11647, variable, limited between 0.000 and 0.500
C 3 = 0.22081, variable, limited between 0.000 and 0.500
C 4 = 0, fixed
*****
Apertures
A 4 = 1.0000, fixed
*****
Parameter Functions
not specified
*****
Columns in the data file and links to nodes
Node number 1 ----> temperature "Tis_back"
Node number 4 ----> temperature "Tis_back"
Node number 4 ----> Flux "HF_back"
*****
Outputs
No.1: Flux "HF_back" at node 4, weight = 1.00
No.2: Not specified
No.3: Not specified
*****
Initial conditions
*****
Initial temperatures were identified.

```

```

-----
Results
-----
Iterations
D downhill Simplex Method: 31800
Monte Carlo Method: 972710
Total number of iterations: 1004510
Last improvement at step: 943995
-----
Residual at end of calculation : 0.64307645 W
-----
Parameters
Par. 1 : H 03-02 = 2.722 W/K ± 3.4 %
Par. 2 : H 01-02 = 0.617 W/K ± 0.8 %
Par. 3 : H 04-03 = 38.762 W/K ± 4.0 %
Par. 4 : C 02 = 0.0194 MJ/K ± 2.8 %
Par. 5 : C 03 = 0.0370 MJ/K ± 1.8 %
Par. 6 : T 02 = -19.906 °C ± 100 %
Par. 7 : T 03 = -19.952 °C ± 100 %
-----
UA and gk
Interior node: Node number 4
Exterior node: Node number 1
Column with vertical radiation: not specified
-----
UA and gk
Interior node: Node number 4
Exterior node: Node number 1
Column with vertical radiation: not specified
UA = 0.490 W/K ± 0.1 %
gk = not calculable
-----
Cross - Correlation
-----

```

	H 03-02	H 01-02	H 04-03	C 02	C 03
H 03-02	1.0000	-0.6792	0.0233	0.0205	-0.3329
H 01-02	-0.6792	1.0000	-0.0000	-0.0098	0.3828
H 04-03	0.0233	-0.0000	1.0000	0.2362	-0.2504
C 02	0.0205	-0.0098	0.2362	1.0000	-0.4043
C 03	-0.3329	0.3828	-0.2504	-0.4043	1.0000

SS21

17

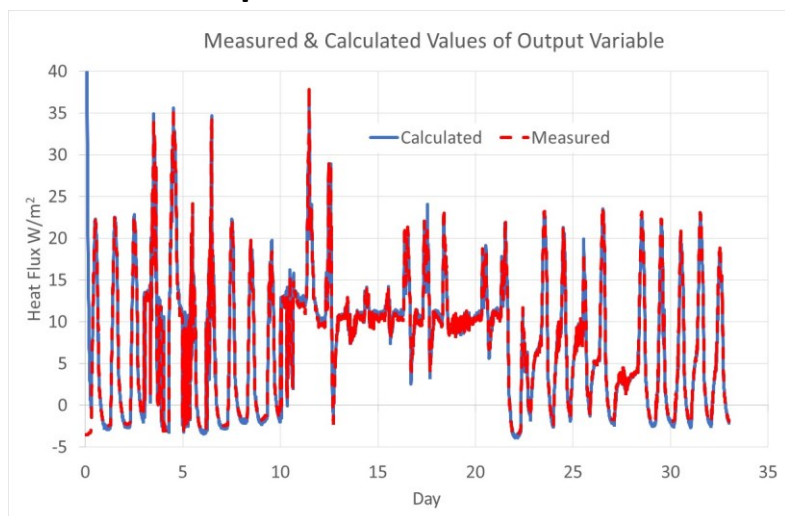
17

Results - Output File *.res gives measured & calculated values of output variable

```

Back_10min-5 - Notepad
File Edit Format View Help
Day      Calc. 1  Meas. 1
0.0069444 1122.4832 -3.5312
0.0138889 710.7753 -3.5433
0.0208333 461.6966 -3.5464
0.0277778 309.8872 -3.5555
0.0347222 216.0325 -3.5646
0.0416667 157.2057 -3.5706
0.0486111 119.2652 -3.5676
0.0555556 94.4965 -3.5433
0.0625000 77.8772 -3.5585
0.0694444 65.5455 -3.5706
0.0763889 56.3539 -3.5494
0.0833333 49.1957 -3.5585
0.0902778 43.4346 -3.5555
0.0972222 38.9503 -3.5525
0.1041667 34.7030 -3.5494
0.1111111 31.0022 -3.5433
0.1180556 27.7674 -3.5191
0.1250000 24.9462 -3.5100
0.1319444 22.8053 -3.5009
0.1388889 20.2331 -3.4888
0.1458333 17.9165 -3.4888
0.1527778 16.0493 -3.4676
0.1597222 14.3594 -3.4646
0.1666667 12.9064 -3.4465

```



SS21

18

18

Save Model

A final option is to run Error Propagation:

LORD 3.21

UA and gA | Functions | Limits | Initial conditions | OEM/PEM | Results | Output graphics | Statistics | Error propagation

Name of input	Uncertainty	unit	consider ?	UA +	UA -	gA +	gA -	d UA	d gA
EXTERNAL	0.500	K	yes	2.406	2.126	---	---	0.140	---
INTERNAL	0.500	K	yes	2.126	2.406	---	---	0.140	---
HF_Glazing	5.000	%	yes	2.371	2.145	---	---	0.113	---

Actual Residual : 0.902 W

Load model

Save model

Start

Help

End

Results with undisturbed inputs:
 UA = 2.258 W/K
 gA = not calculable

Total error (root mean square):
 d UA = 0.228 W/K (10.1 %)
 d gA = not calculable

Start Error propagation

Stop Error propagation

SS21

19

19

Using LORD for Simulation/Validation

- Example: validate results from one part of a data series on another part – identify model on Series 16 and apply to Series 18.
- Run LORD for Series 16 only.
- Obtain results & save model.
- Fix all parameters.
- Set initial conditions.

Conductances [W/K]	Capacitances [MJ/K]	Apertures
H 4-3 = 23.890, fixed	C 1 = 0, fixed	A 4 = 1.0000, fixed
H 3-2 = 0.74170, fixed	C 2 = 0.090770, fixed	
H 2-1 = 1.6260, fixed	C 3 = 0.28090, fixed	
	C 4 = 0, fixed	

- ☐ identified like variable parameters
- ☐ let constant at T = 20 °C
- ☒ let constant at their actual values

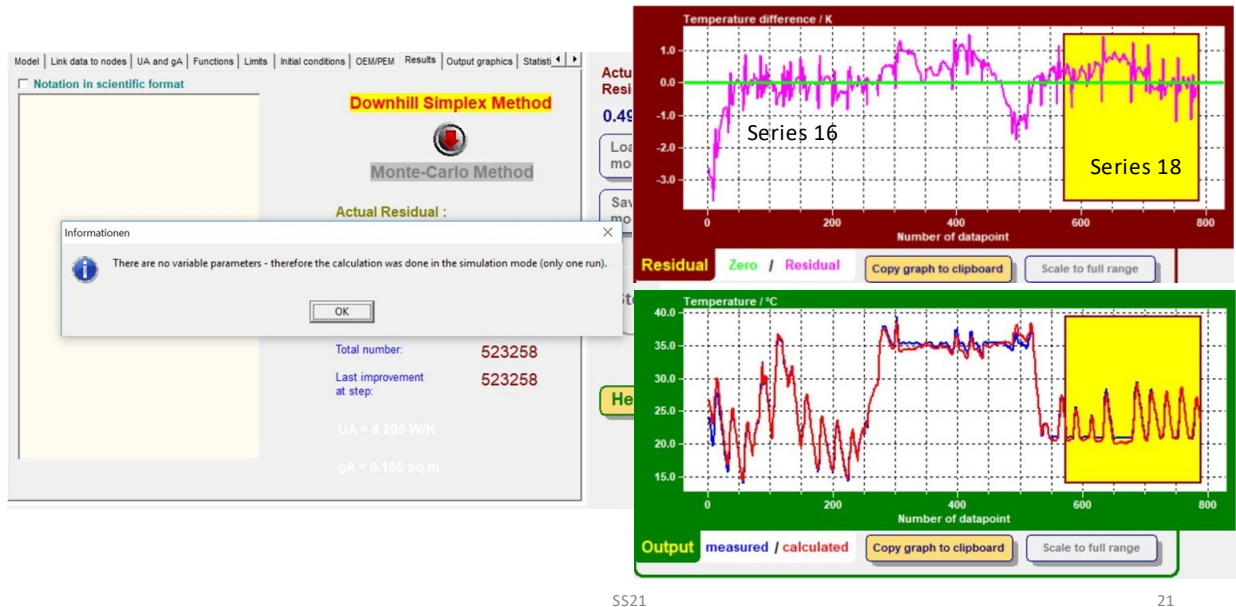
- Move window over Series 18.
- Run LORD.

SS21

20

20

Using LORD for Simulation/Validation



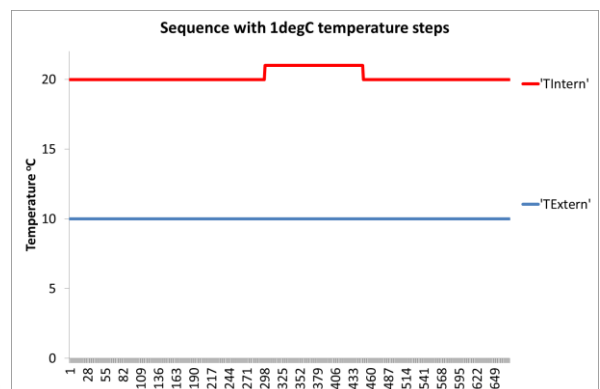
SS21

21

21

Simulation mode – time constants

- Run LORD with data set
- Save model when satisfied with results
- Create simulated data file:
 - heat flux as original file (which is not used in next step using LORD in simulation mode)
 - **with fixed external temperature**
 - **fixed internal temperature with a 1degC step change....**

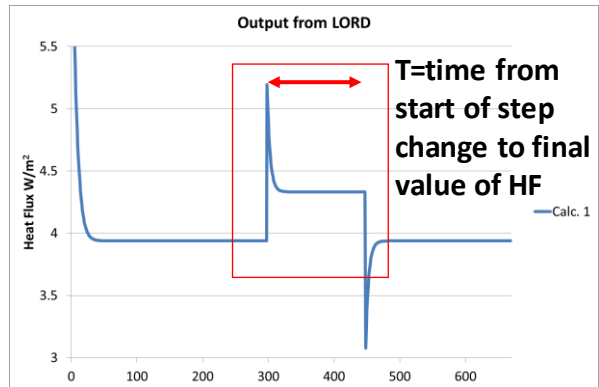


SS21

22

Simulation mode – time constants

- Open the simulated data file.
- Load the model used previously.
- Fix the parameters in the model.
- Fix the initial conditions.
- Set the output to Heat Flux.
- Run LORD
 - it will run in simulation mode.
- Open *****.res** file in Excel
- Find period corresponding to step change..



SS21

23

23

Time Constants and Capacitance

$T = 47$ hours

Time constant = τ or 3τ

$\tau = 63.212\% \times T = 29.7$ hours

$3\tau = 95\% \times T = 44.6$ hours

The Resistance of the model = $2.54 \text{ m}^2\text{K/W}$

Capacitance = Time Constant/ R

For τ : Capacitance = **11.7** Wh/Km²

For 3τ : Capacitance = **17.6** Wh/Km²

There are other methods of obtaining the capacitance

SS21

24

24

Application of LORD to Real Data

- Firstly the data must be processed for input in LORD
 - ❑ Check integrity of data – plots!
 - Missing data?
 - Anomalies?
 - ❑ What data interval to use? *Example of PSA Series 16-18 data follows.*
 - ❑ Etc.

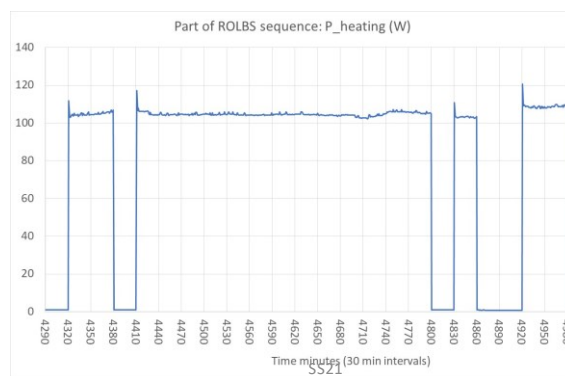
SS21

25

25

What is the optimum data interval in order *not* to lose dynamic information?

- Data are provided at 1 minute intervals (too much information – too long computation time?)
- The ROLBS sequence in Series 16 is based on 30 minute periods:



26

26

- Maximum interval to include all dynamic information is 30 minutes,
- Maybe better to use 10 minute averages.
- Check data to identify start of ROLBS:

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z	AA	AY	AZ
09/12/2013 01:21	4402																											
09/12/2013 01:22	4403																											
09/12/2013 01:23	4404																											
09/12/2013 01:24	4405																											
09/12/2013 01:25	4406																											
09/12/2013 01:26	4407																											
09/12/2013 01:27	4408																											
09/12/2013 01:28	4409																											
09/12/2013 01:29	4410																											
09/12/2013 01:30	4411																											
09/12/2013 01:31	4412																											
09/12/2013 01:32	4413																											
09/12/2013 01:33	4414																											
09/12/2013 01:34	4415																											
09/12/2013 01:35	4416																											
09/12/2013 01:36	4417																											
09/12/2013 01:37	4418																											
09/12/2013 01:38	4419																											

Inspect data: Sequence changes on the hour or half hour.

Therefore start averaging at the beginning of Series 16 at 6/12/13 00:00

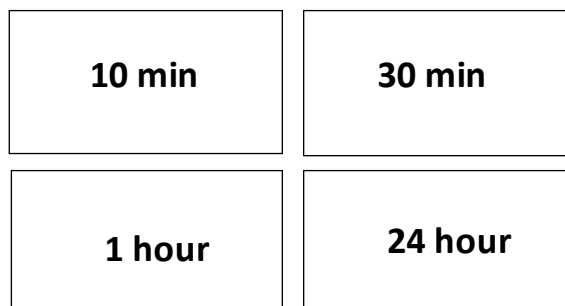
This captures all the dynamic information.

SS21

27

27

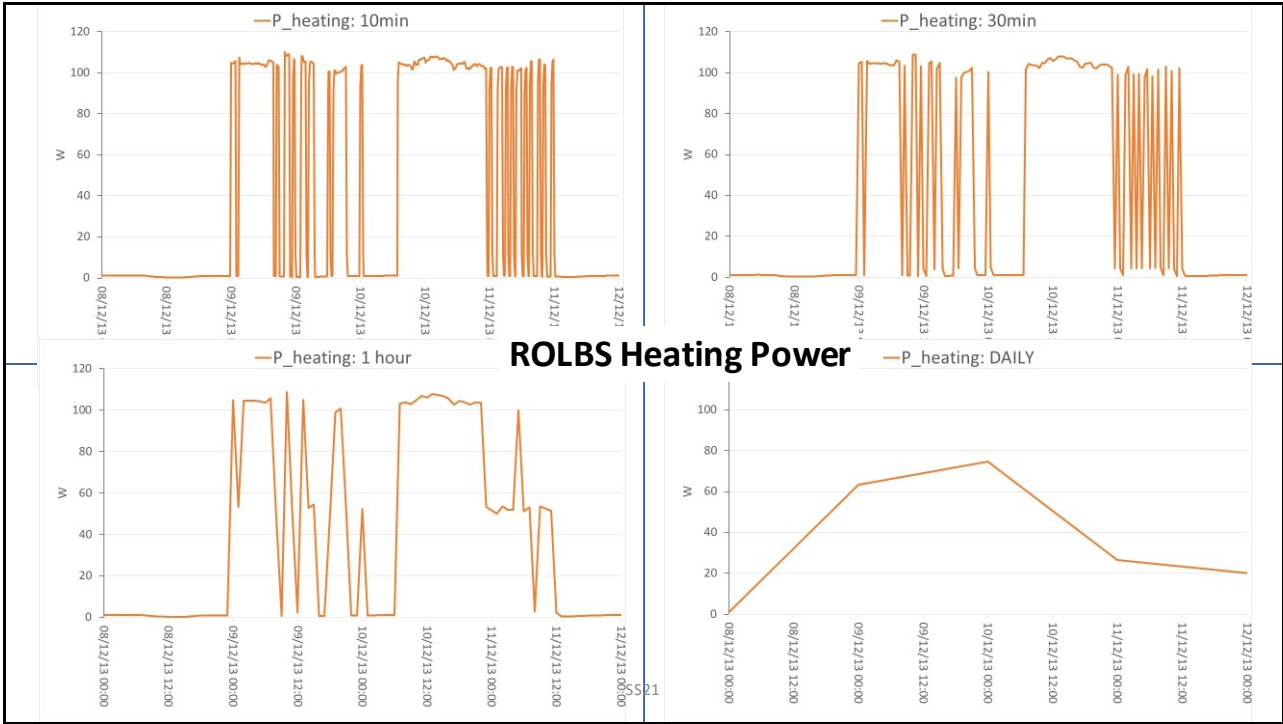
The following figures show the effect of different averaging periods....



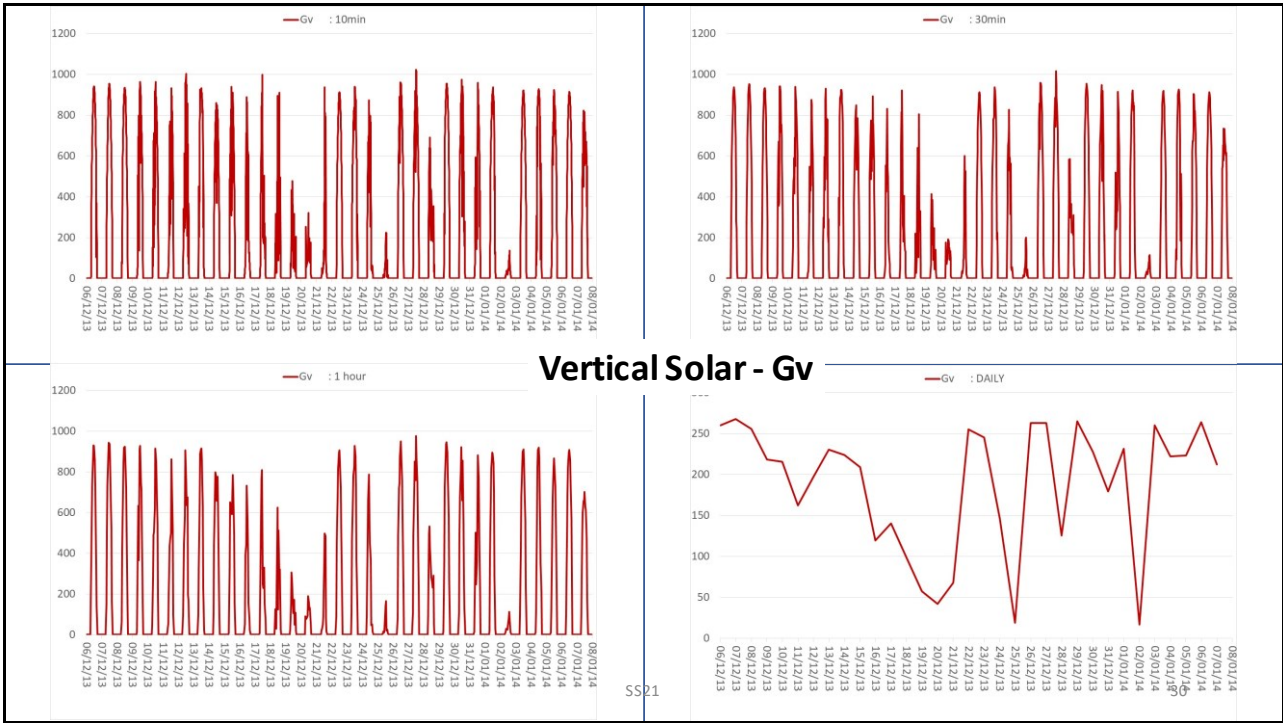
SS21

28

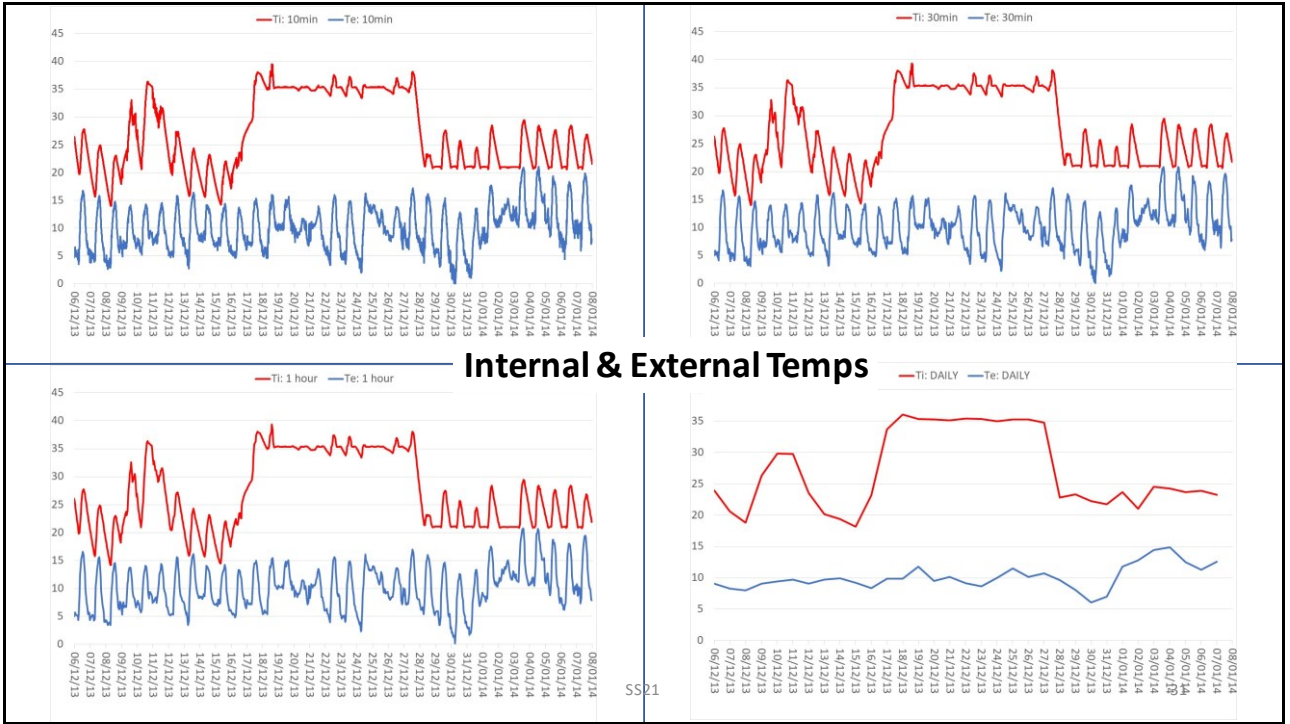
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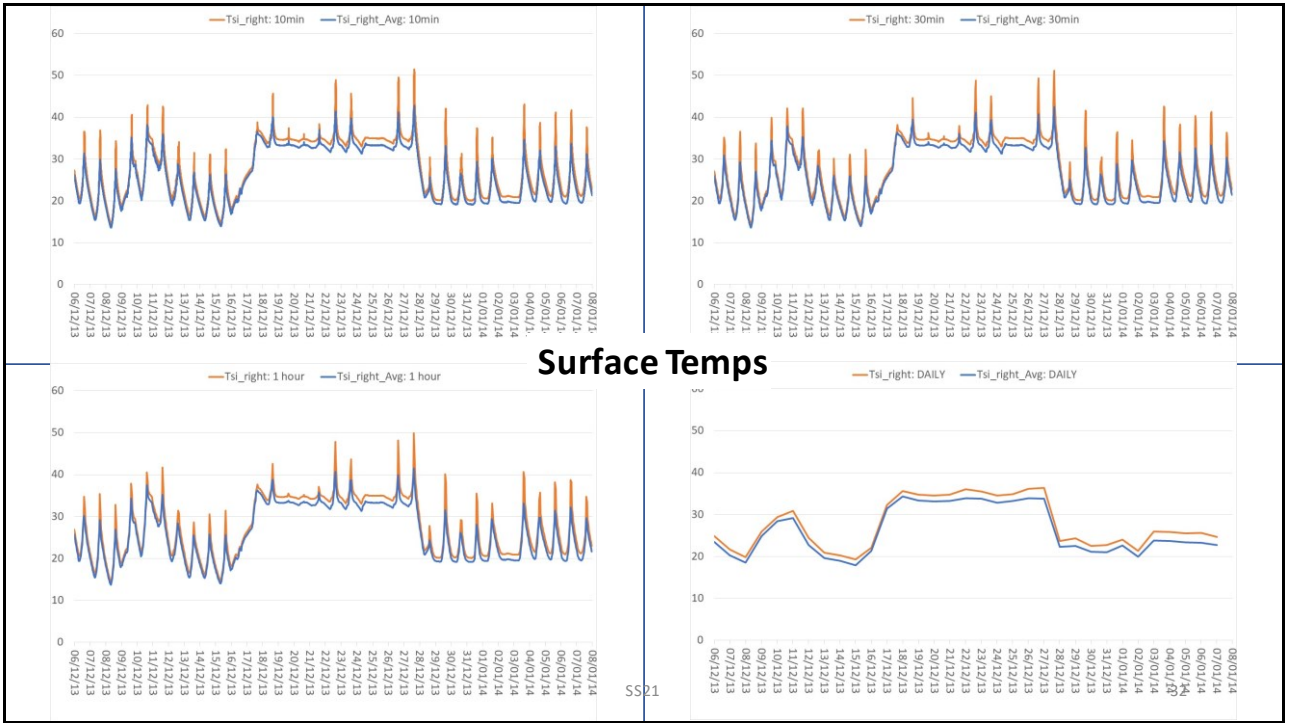
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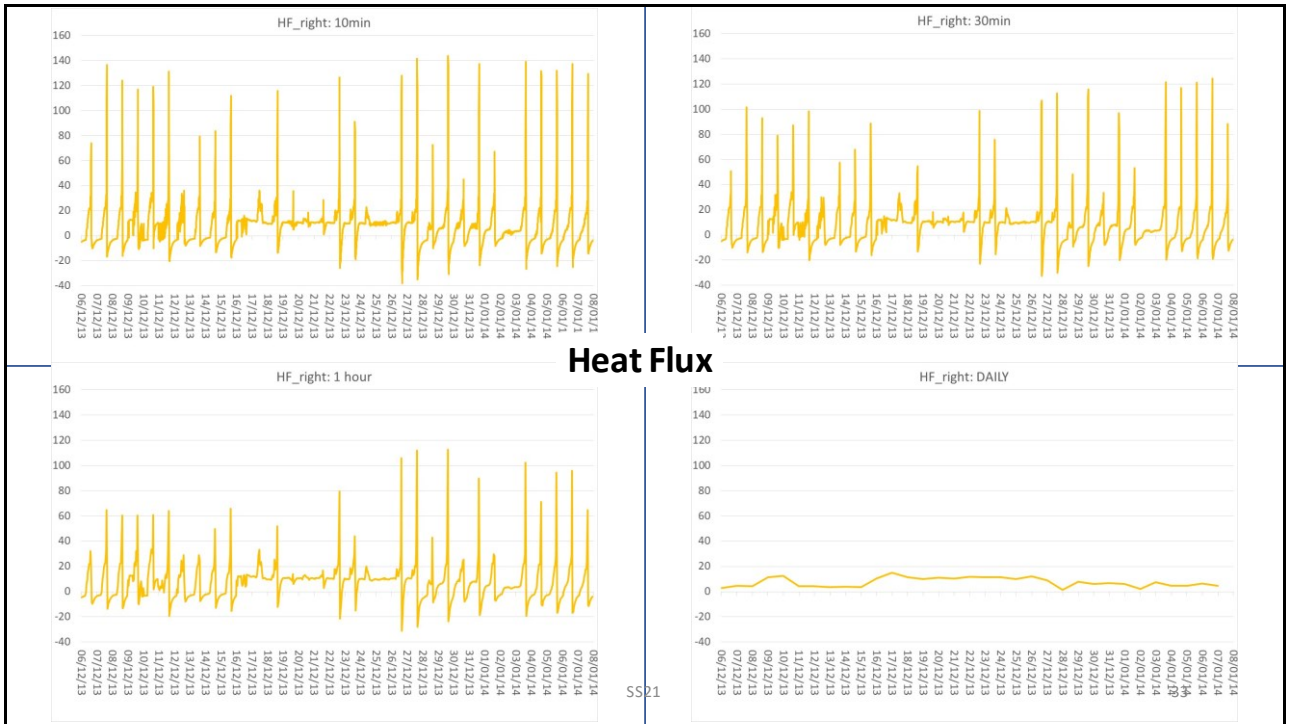
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31



32



33

Applying LORD to Heat Flux Measurements from PSA data

- Firstly it is helpful to estimate results by *simple averaging* before running LORD on data.
- I've tried three approaches using the different temperatures available.....
- These give a good idea of the U-value result(s) you should be aiming for by identification.

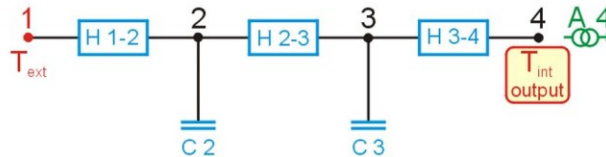
U-value based on Tsi, Tse & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.44	0.46	0.41	0.45	0.53
Series 16	0.47	0.48	0.42	0.48	0.57
Series 17	0.45	0.45	0.42	0.45	0.48
Series 18	0.41	0.43	0.37	0.42	0.55
U-value based on Ti, Te & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.46	0.45	0.44	0.52	0.55
Series 16	0.49	0.49	0.46	0.56	0.61
Series 17	0.45	0.44	0.44	0.49	0.47
Series 18	0.44	0.44	0.43	0.50	0.59
U-value based on Tsi_Avg, Tse & HF					
	Left	Back	Right	Ceiling	Floor
ALL Data	0.47	0.46	0.44	0.48	0.60
Series 16	0.51	0.49	0.46	0.52	0.67
Series 17	0.46	0.45	0.45	0.49	0.52
Series 18	0.45	0.44	0.42	0.45	0.65

SS21

34

Using LORD

- The rear wall is used as an example.
- Use the basic 4 node model.

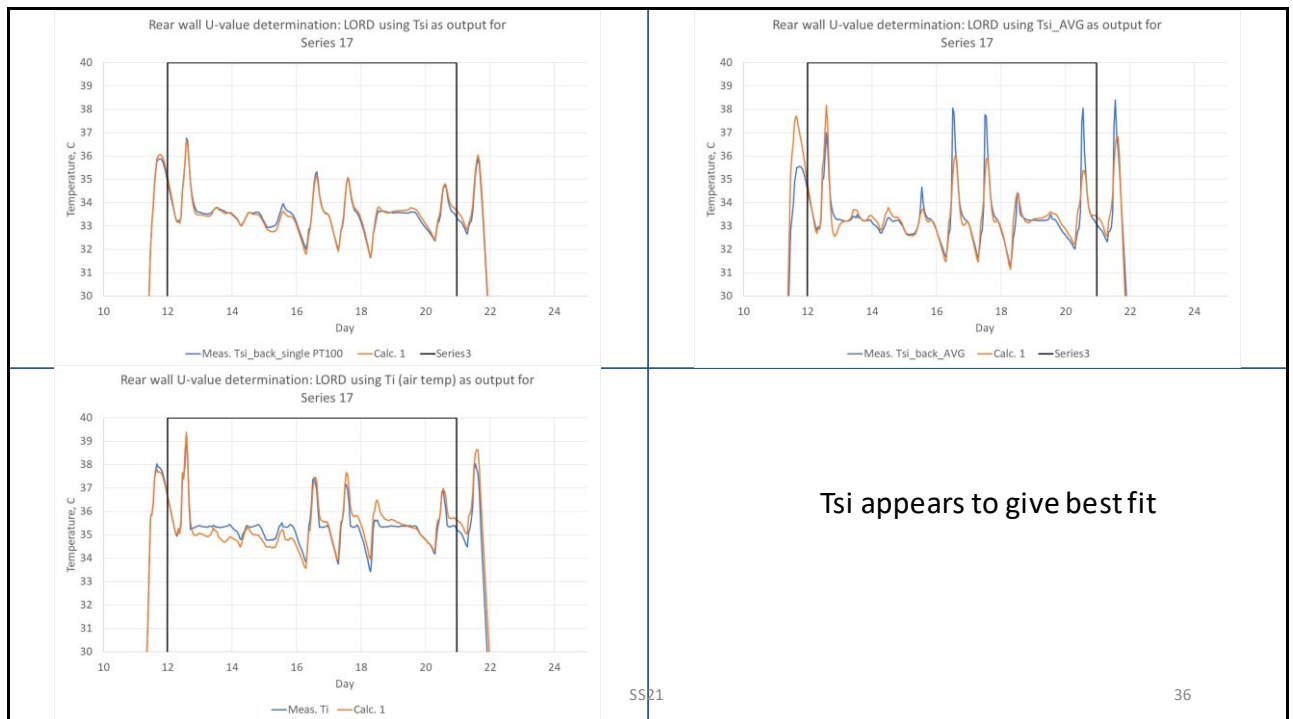


- I've used the external surface temperature T_{se} and the PT100 internal temperature T_{si} because it is more local to heat flux sensor.
- I tried T_{si_Avg} and T_i , however T_{si} produced better results – lower residuals.

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35

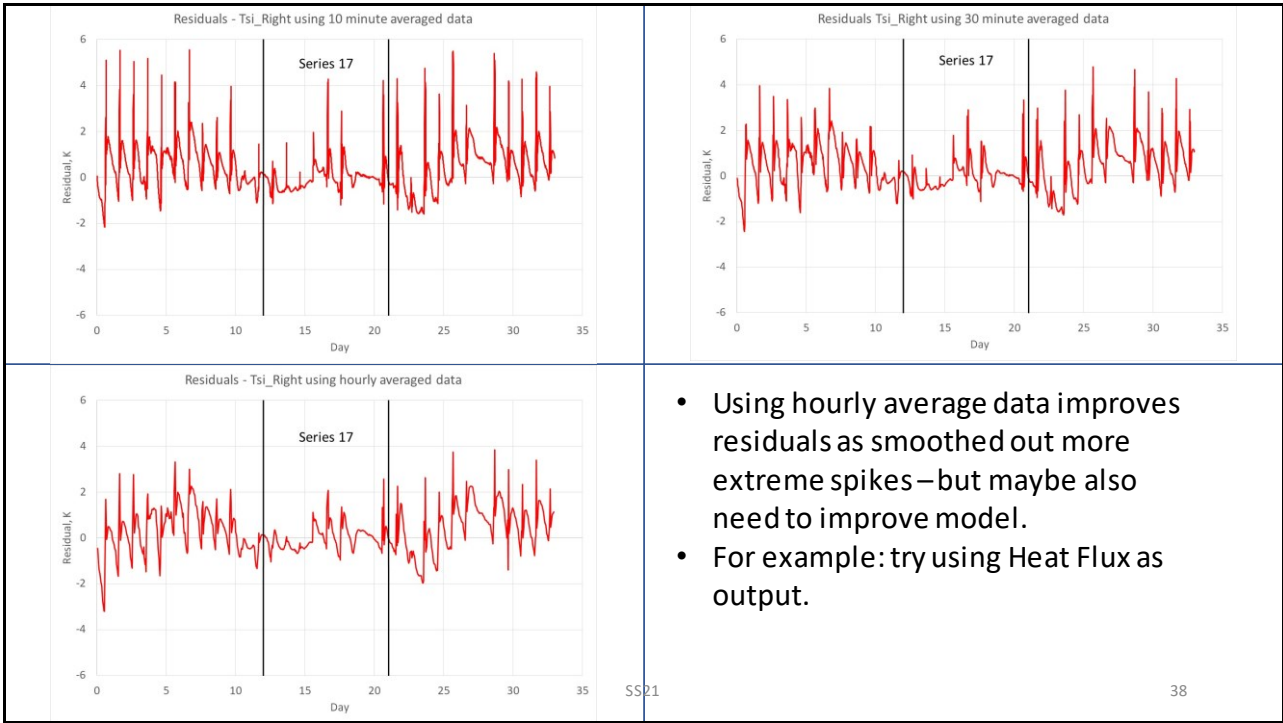
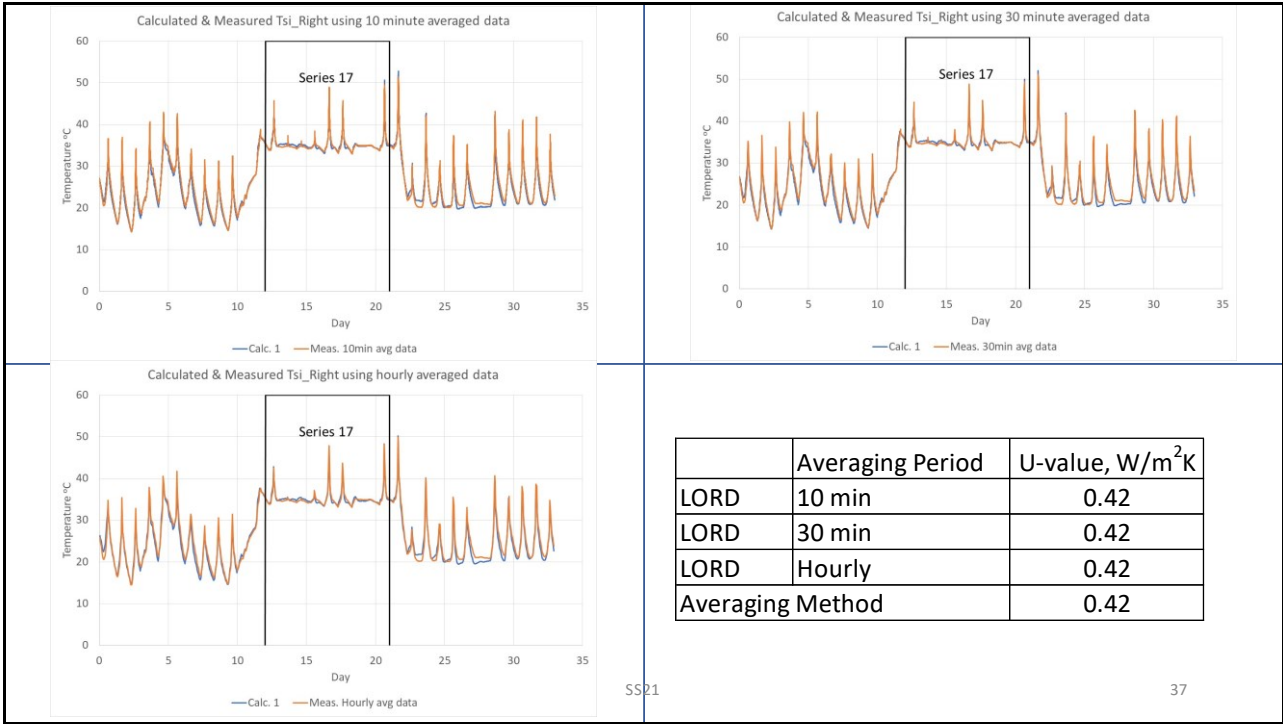
35



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36

36



UA- & gA-values for whole test cell from Series 16-18 or 'Co-heating' test of a building

- For the heat flux measurements we can easily get an idea of the U-value by the *averaging method*, however this is not possible for UA- & gA-values.
- For steady state conditions, the electrical heat input to maintain a constant internal temperature within the test cell or building, will increase when the outside temperature falls and decrease when the solar radiation rises (in actuality these are always fluctuating, but dampened by the thermal inertia).
- However, neither the heat loss coefficient, nor the solar heat gain factor of the building envelope can be measured directly.

SS21

39

39

UA & gA

- But estimates can be made using the daily average data with ***Siviour Analysis*** for Series 16-18.....

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40

40

What is Siviour Analysis?

Daily averages (or longer) are produced.

$$P_{\text{heating}} = UA \times \Delta T - gA \times Gv$$

Dividing by ΔT gives

$$\frac{P_{\text{heating}}}{\Delta T} = UA - gA \times \frac{Gv}{\Delta T}$$

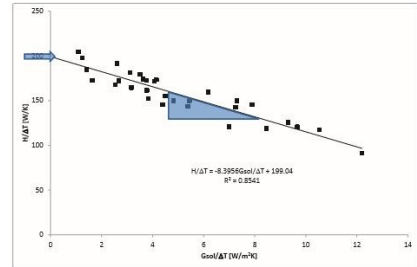


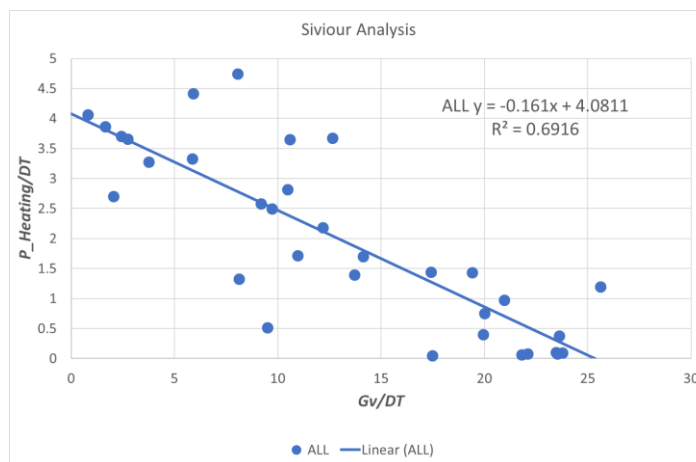
Figure A2: Example of X-Y plot of co-heating test data (Siviour analysis). The intercept of the linear regression line is the whole house heat loss coefficient and the slope is the solar gain factor

SS21

41

41

All data Series 16-18

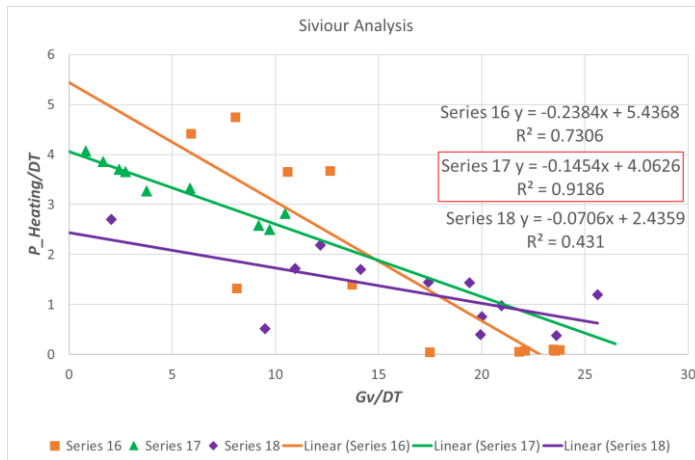


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42

42

Divide into 3 series



Series 17 gives the best fit:
 $UA = 4.06 \text{ W/K}$
 $gA = 0.145 \text{ m}^2$

Best 'steady state' data series with high ΔT

This suggest that the data series would *possibly* give good results for steady state parameters using LORD, etc.

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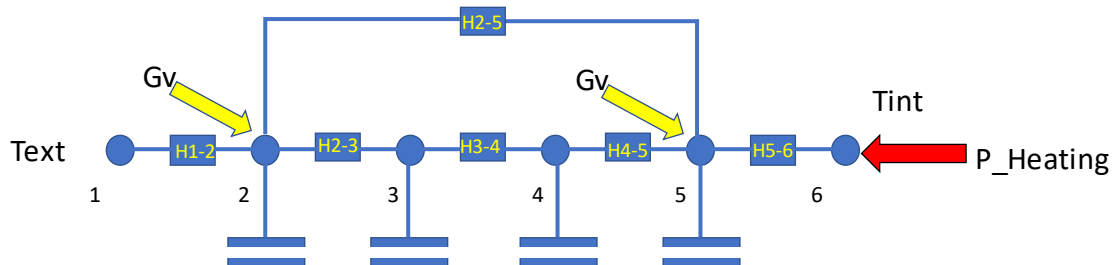
43

43

'Whole Building' model

- Represent in LORD with six nodes (could be less!):

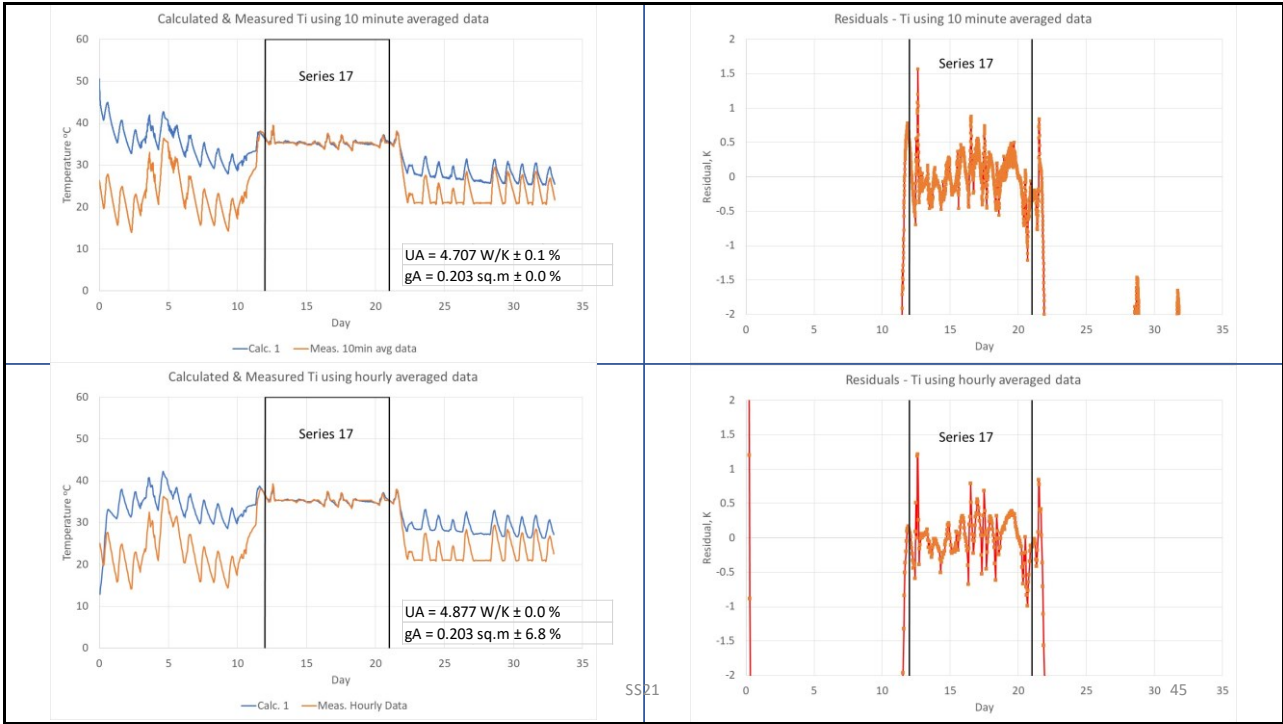
The additional parallel conductance H2-5 connected between node 2 and 5 allows for thermal conduction without storage (e.g. a window).



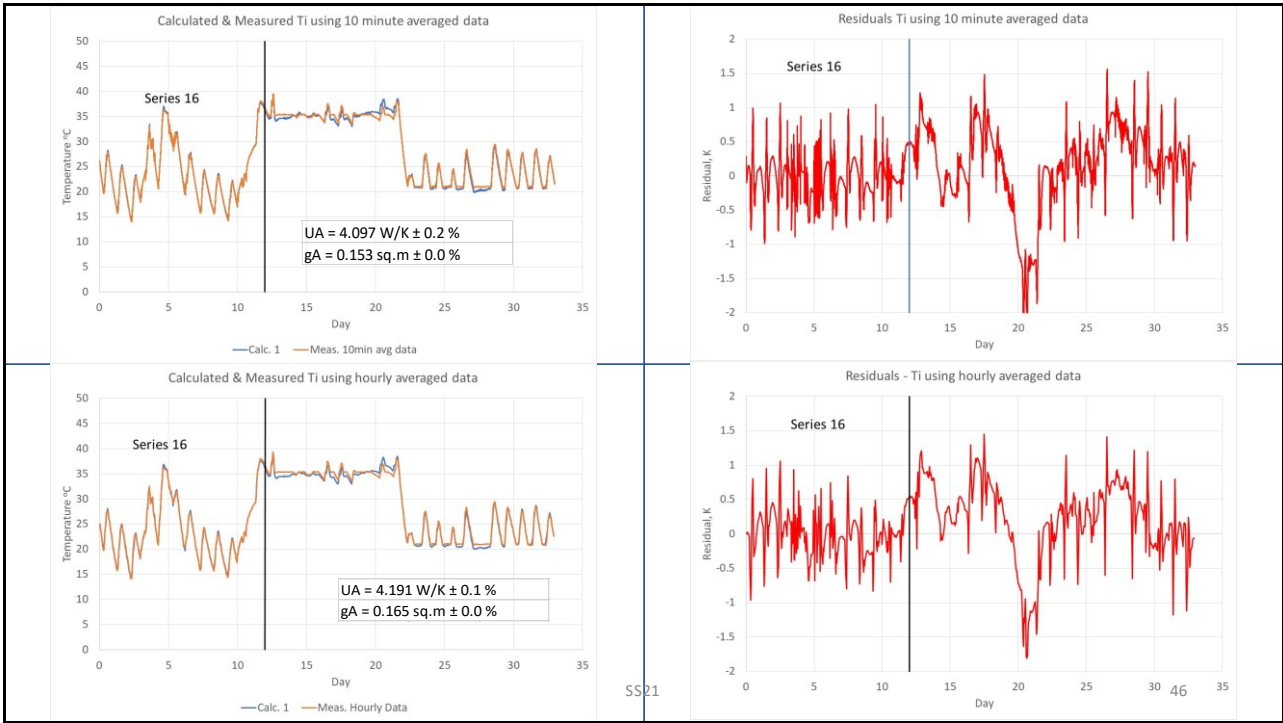
SS21

44

44



45



46

Results

- Expected the more steady state Series 17 would give good results.
- However UA- & gA-values using Series 17 are high.
- Also the fit of the model to the rest of the data (Series 16 & 18) is poor.
- Series 16 gives better results and overall a better fit to *all* data.
- Do we use 10min or hourly data?
- Are there problems with high frequency data using LORD?
- Try different model?

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47

47

Comments & Conclusions

- Important to understand the physical system, for example, the construction of the PSA test cell and sensor locations.
- Plot the data – check for integrity.
- Use simple averaging or Siviour analysis to estimate results prior to using identification techniques.
- Select suitable data averaging period, particularly for dynamic test sequences.
- Compare different parts of test sequences.
- Possible to estimate time constants using ‘simulation’ mode.

SS21

48

48

Useful Reference

- Baker P.H. and van Dijk H.A.L. PASLINK and dynamic outdoor testing of building components. Building and Environment Vol.43 pp143–151, 2008

SS21

49

49

Thank you Maria for your presentation

Thank you all for attending today's webinar

You can send further questions you might have, via email to

Hans Bloem at: hans.bloem@inive.org

The Webinar will now close.

SS21

50

50